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Polyethylene and Polypropylene Nanocomposites Based on Polymerically- Modified Clay Containing Alkylstyrene Units

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Abstract

Sodium montmorillonite was modified with a new polymeric surfactant. The high molecular weight of the surfactant appears to have led to incomplete cation exchange of the clays, but did promote nanocomposite formation with polyethylene and polypropylene. X-ray diffraction combined with transmission electron microscopy revealed a mixed nanocomposite morphology. The thermal stability of the nanocomposites was evaluated by thermogravimetric analysis, while flammability of the nanocomposites was evaluated by cone calorimetry. A significant 40% reduction in peak heat release rate was observed at 10% organo-clay (3% inorganic clay) loading with an even higher 50% reduction at a loading level of 16% modified clay (5% inorganic clay). Despite possible plasticization effects by the polymers used as an organic modification for the clays, the mechanical properties such as Young's modulus and elongation were not severely impacted by the nanocomposite formation.

Keywords

Nanocomposites, Polymeric surfactant, Polyethylene

1. Introduction

Polymer/clay nanocomposites are of high interest, since low inorganic clay loading levels can lead to significant improvement in many properties [\[1\]](#), [\[2\]](#), [\[2\]\(a\)](#), [\[2\]\(b\)](#), [\[3\]](#), such as fire retardancy (FR), mechanical, and barrier properties. A significant amount of work has been focused on the fire retardancy of polymer/clay nanocomposites [\[4\]](#), [\[5\]](#), [\[6\]](#), as an alternative for, or in addition to, traditional FR-additives. Previous work has shown that 3–10% organically-modified clay dispersed in the polymer matrix can reduce the heat release rate (HRR) from 30% to 70% and it also provides mechanical reinforcement and a non-dripping character to the combustion and the reduction in the peak heat release rate is very polymer dependent. In addition, the synergistic effect between clay and conventional FR-additives permits achieving fire retardancy with a substantially reduced amount of conventional FR-additives [\[4\]](#), [\[7\]](#).

To successfully fabricate polymer/clay nanocomposites, the inherent immiscibility between most organic polymers and the inorganic clay filler must be overcome. Typically, alkyl based quaternary ammonium salts are used to exchange the inorganic cations in the clay galleries, rendering organophilicity to the clay particles [\[12\]](#). For non-polar polymers, besides the organic modification of the clays with ammonium salts, a polymeric compatibilizer is often required to obtain well-dispersed systems [\[8\]](#), [\[8\]\(a\)](#), [\[8\]\(b\)](#), [\[9\]](#), if the nanocomposites are to be made through melt processing [\[8a\]](#). The normal condition is to use the polyolefin-*graft*-maleic anhydride as a compatibilizer, since reaction may occur between a properly functionalized surfactant and the maleic anhydride to form the nanocomposite. Thus, one initially prepares a masterbatch containing PP-*g*-MA or PE-*g*-MA together with the clay and then this is combined with the virgin polyolefin to achieve the required clay content.

Recent work from this laboratory showed the successful use of oligomeric surfactants to modify clay by the ion-exchange method [\[10\]](#), [\[10\]\(a\)](#), [\[10\]\(b\)](#), [\[10\]\(c\)](#), [\[11\]](#), [\[11\]\(a\)](#), [\[11\]\(b\)](#), [\[11\]\(c\)](#), [\[11\]\(d\)](#). Generally, the oligomers are random copolymers of vinylbenzyl chloride (VBC) and another monomer, such as styrene, methyl methacrylate, lauryl acrylate, etc. Cationic surfactants are formed by reacting an amine with benzylchloride. The resulting oligomerically-modified clays contain a much higher organic content than the typical alkyl-ammonium modified clays. These oligomerically-modified clays can be utilized to form nanocomposites with either polar or non-polar polymers. Typically, the *d*-spacing prior to nanocomposite formation is around 4 nm [\[12\]](#), and polymer chains can intercalate into the clay gallery sometimes without further expansion being required. Most of the nanocomposites based on the oligomerically-modified clays exhibit good nano-dispersion, *i.e.*, either intercalation or delamination.

Oligomerically-modified clays containing lauryl acrylate units [\[11\]](#), [\[11\]\(a\)](#), [\[11\]\(b\)](#), [\[11\]\(c\)](#), [\[11\]\(d\)](#) possess higher thermal stability than the common ammonium-based organically-modified clays and can be processed above 300 °C. Nanocomposites based on these clays can be melt blended in a relatively short time (3–5 min), which may be attractive to industry. Since the oligomerically-modified clay contains a large organic content, a considerable amount of oligomer will inevitably be introduced to the nanocomposite, which can act as a plasticizer for the polymer matrix. Functional groups in the oligomer, such as the ester group in lauryl clay (*cf.* clay modified by a copolymer of lauryl acrylate and VBC) and triclays (*cf.* clay modified by a terpolymer of lauryl acrylate, styrene and VBC) [\[11\]](#), could be deleterious when the nanocomposites are subjected to acidic or basic condition. In addition, when the surfactant contains polar moieties, such as carboxy groups, the compatibility with the non-polar polyethylene and polypropylene is not as good as is necessary to achieve good nano-dispersion of the clay in the polymer. Among these oligomerically-modified clays, triclays [\[11\]](#), [\[11\]\(a\)](#), [\[11\]\(b\)](#), [\[11\]\(c\)](#), [\[11\]\(d\)](#) exhibited the best reduction in the peak heat release rate (PHRR), as measured by cone calorimetry.

In this work, the ester group has been avoided and, instead, a long alkyl chain was attached to the styrene to determine whether an alkylstyrene surfactant is suitable as an organic modification for clays. In order to reduce any plasticizing effect, a polymeric surfactant, rather than a lower molecular weight oligomer, has been used. This new polymeric surfactant, containing 4-nonylstyrene, was used to modify sodium

montmorillonite, and was subsequently melt blended with polyethylene (PE) and polypropylene (PP) to prepare nanocomposites.

2. Experimental

2.1. Materials

Polyethylene (LDPE), Petrothene NA960000, was supplied by Equistar Chemical Company. Isotactic polypropylene (melt index 230 °C/2.16 kg, 4 g/10 min), vinylbenzyl chloride, 2,2'-azobisisobutyronitrile (AIBN), and lithium wire were acquired from Aldrich Chemical Company. 1-Bromooctane was acquired from Lancaster. Sodium montmorillonite (Na Cloisite, with CEC $\cong$ 0.95 meq/g) was provided by Southern Clay Products, Inc.

2.2. Synthesis of 4-nonylstyrene

Lithium wire (1.4 g, 0.20 mol) was placed in a 250 ml three-neck round bottom flask containing 50 ml of dry ether and equipped with an addition funnel. The system was maintained under nitrogen flow and was held at 0 °C using an ice water bath. A few drops of 1-bromobutane were added and stirred until the lithium metal became bright, 19.3 g (0.10 mol) of 1-bromooctane in 100 ml of dry ether was then added drop-wise over a 1 h period. The ice water bath was removed and the system was allowed to warm to room temperature and was held at that temperature for 30 min. The ether solution of octyllithium was transferred by syringe, drop-wise, to a separate flask containing a solution of 14.5 g (0.095 mol) of vinylbenzyl chloride in 100 ml of dry THF. The solution was stirred under nitrogen purge for 1 h, and then 1 M HCl was added to hydrolyze any remaining lithium reagents. The oil layer was extracted with ether followed by column chromatographic separation (hexane/ethyl acetate 90:10). Colorless 4-nonylstyrene (18.6 g, 81% yield) was recovered. The identity of the nonylstyrene is clearly established by NMR spectroscopy. ^1H NMR (CDCl_3 , ppm): 7.32 (d, J = 9 Hz, 2H, ArH), 7.15 (d, J = 9 Hz, 2H, ArH), 6.68 (dd, J = 12, 18 Hz, 1H, ArCH-), 5.70 (d, J = 18 Hz, 1H, ArCHCH₂cis), 5.17 (d, J = 12 Hz, 1H, ArCHCH₂trans), 2.58 (t, J = 7 Hz, 2H, ArCH₂-), 1.57 (quintet, J = 7 Hz, 2H, ArCH₂CH₂-), 1.30 (m, 12H, -(CH₂)₆-), 0.88 (t, J = 6 Hz, 3H, -CH₃).

2.3. Copolymer and its ammonium salt

4-Nonylstyrene (46 g, 0.20 mol) and vinylbenzyl chloride (3.1 g, 0.02 mol) were dissolved in 100 ml of THF in a 250 ml flask. The solution was magnetically stirred for 10 min, and heated to gentle reflux, then 0.32 g (2.0 mmol) of AIBN was added to initiate the polymerization and the system was maintained at reflux for 12 h. The copolymer was precipitated by pouring the solution into 500 ml of methanol and 45 g of copolymer were collected after filtration followed by overnight drying in a vacuum oven at 70–80 °C. The molecular weight of the polymer was characterized by gel permeation chromatography; the number average molecular weight is 31,000 with a polymer dispersity index of 3.1. ^1H NMR (CDCl_3 , ppm): 7.14 (br, 22H, ArH), 6.72 (br, 22H, ArH), 4.47 (br, 2H, ArCH₂Cl), 2.56 (br, 20H, ArCH₂-), 2.33 (br, 11H, ArCH-), 1.90 (br, 22H, ArCHCH₂-), 1.63 (br, 20H, ArCH₂CH₂-), 1.29 (br, 120H, -(CH₂)₆-), 0.89 (t, 30H, -CH₃). The NMR data are consistent with a copolymer composition of 10:1 ratio of nonylstyrene to vinylbenzyl chloride.

Copolymer (45 g) was first dissolved in 200 ml THF followed by the addition of 4 g of triethylamine and the mixture was stirred at room temperature for 12 h before it was slowly poured into 500 ml of methanol. The polymeric surfactant was collected by filtration and dried overnight in a vacuum oven at 80 °C. There was a new broad peak in the ^1H NMR spectrum at 3.44 ppm, which may be assigned as the methylene group attached to the nitrogen of the ammonium salt, while the methyl group adjacent to the methylene is in the 1.30 ppm region.

2.4. Clay modification

Sodium montmorillonite (15 g) was dispersed in 300 ml of THF/H₂O (50:50) and stirred magnetically for 8 h, while 35 g of surfactant was dissolved in 100 ml THF. An 80 ml portion of the surfactant solution was slowly added to the clay suspension and the system was vigorously stirred for 12 h; subsequently, the remaining surfactant solution was added drop-wise until a precipitate appeared. The precipitate was collected and washed with 500 ml THF/H₂O (50:50). After drying at 80 °C under vacuum, 50 g of polymerically-modified clay was collected for further study.

2.5. Nanocomposite formation

All polymer/clay nanocomposites were prepared by melt-blending in a Brabender Plasticorder at 60 rpm and 185 °C for 5 min; these are the same conditions that have been used in previous studies with PE and PP nanocomposites [10], [10](a), [10](b), [10](c), [11], [11](a), [11](b), [11](c), [11](d). The polymer and the modified clay were charged into the Brabender chamber simultaneously and after 5 min of blending the mixture was removed from the chamber and allowed to cool to room temperature. Table 1 lists the compositions of the nanocomposites.

Table 1. Composition, mass %, of polymer/clay nanocomposites

No.	Polymer (PE or PP)	Polymerically-modified clay	Inorganic clay loading
1	97	3	1
2	90	10	3
3	84	16	5

2.6. Characterization

X-ray diffraction (XRD) was carried out on a Rigaku Geiger Flex, 2-circle powder diffractometer with Cu K α generator at 50 kV and 20 mA, scanning from 1 to 10° at a step value of 0.1°. XRD samples were molded into 20 mm $\times$ 15 mm $\times$ 1 mm plaques. Bright field TEM images were obtained with a JEOL 1200 EXII microscope operated with an accelerating voltage of 80 kV, and equipped with a Tietz F224 digital camera. Thin sections of the nanocomposites were cut from a plaque using a microtome (Leica Ultracut UCT) equipped with a diamond knife; although liquid nitrogen was used prior to microtoming, and multiple sessions of microtoming for each sample were done, all sections obtained were relatively thick (above 500 nm) thus limiting the resolution of the TEM. The sections were transferred to carbon-coated copper grids (200 mesh). No heavy metal staining of sections prior to imaging was necessary, since the contrast between the layered silicate and the polymer matrix was sufficient.

Thermogravimetric analysis (TGA) was performed on a SDT 2960 unit, under 60–80 ml/min nitrogen flow. The samples were first equilibrated at 100 °C and then ramped to 600 °C at a scan rate of 20 °C/min. Temperatures are reproducible to ± 3 °C while the fraction of non-volatile is repeatable to $\pm 2\%$. Cone calorimetry was performed on an Atlas CONE-2 according to ASTM E 1354 under a heat flux of 35 kW/m². Exhaust flow was set at 24 l/s. The spark was continuous for 10 s after ignition. Samples for cone calorimetry were prepared by compression molding into 100 mm $\times$ 100 mm $\times$ 3 mm plaques. Typically, results from cone calorimetry are reproducible to within $\pm 10\%$ [13], [13](a), [13](b). Tensile properties were measured using an MTS Alliance RT/5 tensile test machine at a crosshead speed of 50 mm/min. The reported values are the average of five determinations. Molecular weight was determined using a DAWN EOS MALLS (Wyatt Technologies) coupled with a W-410 RID (Waters Corporation) using Waters Ultrastaygel columns HR4, HR3, HR1 in series; THF was the mobile phase.

3. Results and discussion

3.1. X-ray diffraction

X-ray diffraction (XRD) patterns of the polymerically-modified clay and its PE nanocomposites are shown in Fig. 1. The modified clay displays a strong peak at 2.4°, which is approximately the same as that seen in oligomerically-modified clays (lauryl clay, triclays) containing a long alkyl chain in the monomer unit [11], [11](a), [11](b), [11](c), [11](d), and corresponds to a *d*-spacing of 3.7 nm. There is a very broad feature in the 4–8° 2 θ region, which perhaps implies incomplete ion-exchange, possibly due to the high molecular weight of the surfactant. The XRD patterns of the PE and PP nanocomposites are shown in Fig. 2, Fig. 3. PE and PP nanocomposites have similar XRD patterns at all clay loadings. The broad feature in the 4–8° 2 θ region remains for all the samples, however, the *d*₀₀₁ diffraction peak from the polymerically-modified clay is substantially weakened, denoting that exfoliation or disordering of the clay may have occurred. Thus, the XRD traces suggest that the system contains both an immiscible component (from the broad feature at 4–8°) and a nano-dispersed component.

Fig. 1. XRD pattern of polymerically-modified clay.

Fig. 2. XRD patterns of polyethylene clay nanocomposites.

Fig. 3. XRD patterns of polypropylene clay nanocomposites.

3.2. Transmission electron microscopy

Transmission electron microscopy (TEM) allows for the direct imaging of the filler dispersion, *albeit* in a much smaller region than what is interrogated by XRD. TEM images were obtained for both PE and PP nanocomposites at 3% inorganic clay loading, and are shown in [Fig. 4](#), [Fig. 5](#), respectively. The low magnification images show the presence of extended clay tactoids – in both the PE and PP – nanocomposites, indicating that the majority of the clay platelets are not well dispersed (*cf.* delaminated or exfoliated) in either polymer matrix. The high magnification images do show intercalated structures – and much fewer immiscible formations – within and around the micrometer-sized tactoids, for both PE and PP. These TEM observations are in concert with the XRD results above and, to the extent that they are representative of the composite structure, provide some further insight into the mesoscale (micrometer size) morphology of the composites. However, due to the relative large thickness of the sections imaged, the present TEM study could only qualitatively detect nanoscale structures, without enabling us to derive definitive conclusions at this length scale. Based on the combination of

XRD and TEM, these systems contain clay which is nano-dispersed in the polymer and also clay which exists only as tactoids, *i.e.*, some fraction of the clay is nano-dispersed.

Fig. 4. TEM images of PE nanocomposites at 3% inorganic clay loading.

Fig. 5. TEM images of PP nanocomposites at 3% inorganic clay loading.

3.3. Thermogravimetric analysis

A general limitation with organically-modified clay is the processing temperature. Normally, organically-modified clay should be processed below 200 °C to avoid degradation of the ammonium surfactants [14]. Previous studies have shown that the thermal stability of oligomerically-modified clay is higher than that of the common organically-modified clays. The data acquired from TGA curves include the onset of the degradation, which is usually taken as the temperature at which 10% degradation occurs, $T_{0.1}$, the mid-point temperature of the degradation, $T_{0.5}$, another measure of thermal stability, and the non-volatile residue which remains at 600 °C, denoted as char. For oligomerically-modified clay, $T_{0.1}$ can reach 350 °C and $T_{0.5}$ can reach 400 °C [11], [11](a), [11](b), [11](c), [11](d). The present polymerically-modified clay also exhibits equally good thermal stability, as seen from Fig. 6. The onset temperature is 360 °C and mid-point temperature is 412 °C. Those values are comparable to that of the oligomerically-modified clays. The non-volatile fraction that remains at 600 °C is denoted as char and contains both the polymeric char and the inorganic clay residue. From the TGA curve of the clay itself, there is 30% non-volatile remaining at 600 °C, indicating the inorganic content of the clay. An oligomerically-modified clay which contains an oligomer with a molecular weight of about 5000 also contains about 70% organic and 30% inorganic clay. In this polymerically-modified clay, if there were complete ion-exchange of the inorganic cation for the polymerically-modified cation, the organic content must be substantially higher than 70%, which is a clear indication that there is incomplete exchange, in agreement with the broad feature seen in the XRD traces which was assigned as indicative of incomplete ion-exchange.

Fig. 6. TGA curve of the polymerically-modified clay.

The TGA curves for PE and PP nanocomposites are shown in [Fig. 7](#), [Fig. 8](#) and the corresponding data are listed in [Table 2](#), [Table 3](#). The temperature at 10% degradation, $T_{0.1}$, of the PE nanocomposites shows a similar trend as the PE/oligomerically-modified clay nanocomposites, a higher temperature at low clay loading and a lower temperature at high clay loading. This change is likely due to the lower thermal stability of the surfactant compared to that of the polymers. $T_{0.5}$ shows more than 10 °C enhancement at all clay loadings, while the enhancement for PE clay nanocomposites using the common organically-modified clays is less than 10 °C [\[15\]](#). The thermal stabilities of PP nanocomposites, in terms of the onset of degradation, are more enhanced than the PE nanocomposites; the onset temperature is 45 °C higher for PP nanocomposites at 1% inorganic clay loading compared to unfilled PP. At higher inorganic clay loading, which means more polymeric surfactant was present in the composites, the improvement is 39 °C for PP nanocomposite at 3% inorganic clay loading and 13 °C at 5% inorganic clay loading. $T_{0.5}$ of the PP nanocomposites shows more than 30 °C enhancement at all clay levels. The enhanced thermal stabilities of the PE and PP composites must be attributed to nanocomposite formation. For both PE and PP nanocomposites, the non-volatile fraction at 600 °C is equal to the amount of the inorganic clay in the system, suggesting that there is no polymeric char formed during degradation and all the PE and PP undergo thermal degradation and volatilization.

Fig. 7. TGA curves for polyethylene clay nanocomposites.

Fig. 8. TGA curves for polypropylene clay nanocomposites.

Table 2. TGA data, in nitrogen, for polyethylene and its nanocomposites

PE, wt%	Polymerically-modified clay, mass %	$T_{0.1}$, °C	$T_{0.5}$, °C	Char, wt%
100	—	444	478	0
97	3	462	489	1
90	10	457	491	2
84	16	422	493	5

Table 3. TGA data, in nitrogen, for polypropylene and its nanocomposites

PP, wt%	Polymerically-modified clay, mass %	$T_{0.1}$, °C	$T_{0.5}$, °C	Char, wt%
100	—	389	440	0
97	3	434	470	1
90	10	428	473	3
84	16	412	475	5

3.4. Cone calorimetry

Cone calorimetry is the preferred method to quantify the fire performance for these systems [16]. The parameters determined from cone calorimetry include the time to ignition (t_{ign}); the heat release rate, and especially its peak value (PHRR); the specific extinction area (SEA), a measure of the amount of smoke produced during the combustion; the mass loss rate (MLR); and total heat released (THR). There is a definitive structure–property correlation between the extent of filler nano-dispersion and the PHRR reduction. There is essentially no reduction in PHRR for micro- and macro-composites, while a significant reduction is observed for genuine nanocomposites [13], [13](a), [13](b), [17]. In contrast to TEM, which provides very localized information on the nm/ μm structures, the evaluation of filler dispersion by cone calorimetry is based on a bulk measurement and thus it can yield a more representative, *albeit* indirect, picture of the nano-dispersion. Analysis of cone calorimetric data typically permits one to determine whether the clay is nano-dispersed, but is rather insensitive to the extent of dispersion, *i.e.*, it cannot distinguish between intercalation and exfoliation/delamination.

The cone calorimetry results for the various PE and PP nanocomposites are shown in Table 4, Table 5 and the heat release rate curves for the pure polymers and their nanocomposites are shown graphically in Fig. 9, Fig. 10. PE and PP nanocomposites exhibit similar behavior at the same clay loading. The total heat released is essentially the same for both polymers and their corresponding nanocomposites. There is also no change in the time to ignition for the PP nanocomposites, compared to the unfilled PP. In the case of PE, there is a 15 s increase in the time to ignition for the 3% clay nanocomposites, but at higher clay loadings, the time to ignition is only slightly higher than that of unfilled PE. Time to ignition in polymer/clay nanocomposites is not well-understood but any increase is advantageous. The SEA is increased with increased amount of clay, which is different from our previous work [15]. The increased amount of smoke generation probably arises from the styrene units in the surfactant. At 1% inorganic clay loading, the PHRR reduction is about 20%, whereas essentially no reduction in PHRR is seen when oligomerically-modified clays are used at such low loading [11a].

The PHRR reduction improves to 40% at 3% inorganic loadings, and becomes about 50% at 5% inorganic loading, *i.e.*, the best reduction in PHRR was observed here for the highest clay loading. In previous studies of PE and PP nanocomposites [11], [11](a), [11](b), [11](c), [11](d), 40–60% reduction in PHRR has been observed for nanocomposites containing 5% inorganic clay when the fillers are dispersed at the nanoscale across the polymer matrix. Thus, the nonylstyrene polymeric surfactant gives fire properties comparable to other genuine nanocomposite systems. This strong reduction in PHRR suggests that the clay is well nano-dispersed in the polymer; the conclusion from the XRD–TEM study was that both nano-dispersed and not well-dispersed clays were present (Fig. 4, Fig. 5). Cone calorimetry, a bulk measurement, suggests that there may be a larger proportion of nano-dispersed phase than can be seen from the TEM image and thus may give a better representation of the gross morphology than does TEM.

Table 4. Cone calorimeter data for polyethylene and its nanocomposites

PE	Polymerically-modified clay (inorganic clay)	t_{ign} (s)	PHRR (kW/m ² , % reduction)	MLR (g/s m ²)	SEA (m ² /kg)	THR (MJ/m ²)
100	0	72 ± 3	2067 ± 154	27 ± 2	350 ± 30	100 ± 5
97	3 (1)	87 ± 4	1626 ± 5(21)	25 ± 2	421 ± 20	102 ± 1
90	10 (3)	76 ± 4	1216 ± 64(41)	22 ± 2	501 ± 29	96 ± 4
84	16 (5)	75 ± 5	942 ± 58(54)	17 ± 0	590 ± 8	95 ± 2

t_{ign} , time to ignition; PHRR, peak heat release rate; SEA, specific extinction area; MLR, mass loss rate; THR, total heat released.

Table 5. Cone calorimeter data for polypropylene and its nanocomposites

PP	Polymerically-modified clay (inorganic clay)	t_{ign} , (s)	PHRR (kW/m ² , % reduction)	MLR (g/s m ²)	SEA (m ² /kg)	THR (MJ/m ²)
100	0	53 ± 1	1896 ± 62	26 ± 0	482 ± 57	102 ± 4
97	3 (1)	50 ± 2	1502 ± 119(21)	23 ± 1	574 ± 28	99 ± 5
90	10 (3)	50 ± 3	1200 ± 68(37)	21 ± 1	656 ± 1	94 ± 2
84	16 (5)	51 ± 3	882 ± 74(53)	17 ± 0	731 ± 13	95 ± 4

t_{ign} , time to ignition; PHRR, peak heat release rate; SEA, specific extinction area; MLR, mass loss rate; THR, total heat released.

Fig. 9. Comparison of the heat release rate (HRR) plots for virgin PE and its nanocomposites at 35 kW/m² heat flux.

Fig. 10. Comparison of the heat release rate (HRR) plots for virgin PP and its nanocomposites at 35 kW/m² heat flux.

3.5. Mechanical properties

Most PE and PP nanocomposites based on oligomerically-modified clays show decreased Young's modulus and tensile strength, along with a small decrease in elongation at break. The Young's modulus and tensile strength of the nanocomposites could, in principle, be improved by increasing the inorganic clay content, but this would also lead to a poorer clay dispersion, which would decrease the PHRR reduction and hence the fire performance. The tensile mechanical properties of the present nanocomposites are presented in [Table 6](#), [Table 7](#). For both PE and PP nanocomposites, the tensile strength and Young's modulus are slightly decreased compared to the respective unfilled polymers, which suggest that a plasticizing effect may arise due to the nonyl units attached to the styrene. To diminish the plasticizing effect, the inorganic clay content has to be increased in the modified clay, or employ a different functionalized polymer, such as 0.5–1% maleic anhydride [\[8a\]](#), or ammonium end-terminated polymer [\[18\]](#), [\[18\(a\)\]](#), [\[18\(b\)\]](#). For PE nanocomposites, the elongation shows a small decrease from 450% to 390% when the inorganic clay loading increases from 0% to 5%. For PP nanocomposites, the elongation increases from 380% to 500% when inorganic clay loading increases to 3%. This latter behavior is qualitatively different from that of PP nanocomposites containing montmorillonite clays with most other surfactants [\[8a\]](#).

Table 6. Tensile properties of PE and its nanocomposites

PE	Inorganic clay	Tensile strength (MPa)	Modulus (MPa)	Elongation (%)
100	0	14 ± 2	240 ± 16	457 ± 29
97	1	14 ± 3	210 ± 8	480 ± 22
90	3	13 ± 3	205 ± 9	455 ± 35
84	5	10 ± 2	190 ± 11	390 ± 12

Table 7. Tensile properties of PP and its nanocomposites

PP	Inorganic clay	Tensile strength (MPa)	Modulus (MPa)	Elongation (%)
100	0	34 ± 5	1041 ± 58	378 ± 20
97	1	31 ± 2	1055 ± 40	380 ± 36
90	3	34 ± 6	880 ± 23	500 ± 19
84	5	26 ± 1	832 ± 31	450 ± 12

4. Conclusions

A polymeric surfactant, in the form of a copolymer containing 4-nonylstyrene and vinylbenzyl triethylammonium chloride, was synthesized. When this polymer was used to exchange the sodium cations of montmorillonite clays, a non-uniform structure was observed for the polymerically-modified clays, which was tentatively attributed to the high molecular weight (31,000) of the surfactant. PE and PP nanocomposites were fabricated through melt-blending with the polymerically-modified clay. XRD and TEM indicated a mixed

morphology that was mainly intercalated with some immiscible content. Nanocomposites containing 5% inorganic content exhibited a 50% reduction in PHRR according to cone calorimetry, which strongly suggests that true nanocomposites have been formed. A plasticizing effect of the modified clay on the PE and PP matrices is present, *albeit* to a smaller extent compared to oligomerically-modified clays studied previously. For the PP nanocomposites the elongation at break is improved compared to the unfilled polymer, a behavior which has not been observed with other modified clays.

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