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ANAEROBIC CO-DIGESTION FOR ENHANCED RENEWABLE
ENERGY AND GREEN HOUSE GAS
EMISSION REDUCTION

by

Navaneethan Navaratnam

A Dissertation submitted to the Faculty of the Graduate School,
Marquette University,
in Partial Fulfillment of the Requirements for
the Degree of Doctor of Philosophy

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ABSTRACT
ANAEROBIC CO-DIGESTION FOR ENHANCED RENEWABLE
ENERGY AND GREEN HOUSE GAS
EMISSION REDUCTION

Navaneethan Navaratnam

Marquette University, 2012

The need to develop renewable energy is important for replacing fossil fuel, which is limited in quantity and also tends to increase in price over time. The addition of high strength organic wastes in municipal anaerobic digesters is growing and tends to increase renewable energy production. In addition, conversion of wastes to energy significantly reduces uncontrolled greenhouse gas emissions. Co-digestion of municipal sludge with any combination of wastes can result in synergistic, antagonistic or neutral outcomes. The objectives of this study were to identify potential co-digestates, determine synergistic, antagonistic and neutral effects, determine economic benefits, quantify performance of bench scale co-digesters, identify influence of co-digestion on microbial communities and implement appropriate co-digestion, if warranted, after full-scale testing. A market study was used to identify promising co-digestates. Most promising wastes were determined by biochemical methane potential (BMP) and other testing followed by a simple economic analysis. Performance was investigated using bench-scale digesters receiving synthetic primary sludge with and without co-digestates. Denaturing gradient gel electrophoresis (DGGE) and quantitative polymerase chain reaction (qPCR) analyses were performed on the gene encoding the α subunit of methyl coenzyme M reductase (*mcrA*) to compare methanogen communities among the digesters. One significant band contributing to the greatest difference in banding patterns was excised, cloned, amplified and sequenced. Full-scale co-digestion was conducted using the most promising co-digestate at South Shore Wastewater Reclamation Facility (Oak Creek, WI). Over 80 wastes were identified from 54 facilities within 160 km of an existing municipal digester. A simple economic comparison identified the greatest benefits for seven co-digestates. Methane production rates of two co-digester systems increased by 105% and 66% in comparison to a control system. These increases were great than anticipated based on theoretical methane production from the additional chemical oxygen demand (COD) of the co-digestates. Co-digestion of the most promising wastes with primary sludge was estimated to generate enough electricity to power more than 2500 houses. Synergistic outcomes of co-digestion may be caused by changes in microbial community resulting in more rapid methane production rate and higher specific methanogenic activities of the biomass against acetate, propionate and H_2 as substrates. The presence of *Methanospirillum hungatei* correlated to higher SMAs in the Co-Digester 1 system. In subsequent full-scale testing, acid whey in addition to primary sludge increased methane production by 16 %, biogas methane content by 5%, methane yield per VS destroyed by 9% (from 650 to 710 L CH_4 / kg VS_{destroyed}) and volatile solids removal by 20%. Co-digestion is a promising technology to increase renewable energy production and convert municipal digesters into regional renewable energy facilities.

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Navaneethan Navaratnam

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Chapter 1

Anaerobic co-digestion for increased renewable energy

1.1 Introduction

World energy demand is rapidly increasing with increasing human population, urbanization and modernization (Asif and Muneer, 2007). Most of a countries' energy is delivered by fossil fuels, which are limited in quantity. Moreover, energy generation from fossil fuels can potentially increase greenhouse gas emissions. Therefore, it is important to find alternative energy production strategies such as a renewable energy. Many attempts to produce renewable energy have been made by researchers. These attempts involve wind energy, solar energy biogas energy and other technologies. Biogas energy from waste is an interesting option since it offers two benefits: energy production and waste treatment. Anaerobic digestion is a proven technology to produce biogas from waste.

1.1.1 Anaerobic digestion and anaerobic co-digestion

Anaerobic digestion (AD) is a process for treating organic compounds in wastes and produces biogas. Produced biogas is basically composed of around 65 % methane (CH_4) and 35 % carbon dioxide (CO_2) with trace quantities of potentially corrosive hydrogen sulfide and water vapor. CH_4 can be burned to produce combined heat and power (CHP) as renewable energy. This process relies on microorganisms that break down complex organic compounds into biogas as an end product in the absence of oxygen. Anaerobic digestion is carried out in a series of four main steps involving different groups of microorganisms: hydrolytic bacteria, acidogenic bacteria, acetogenic

bacteria and methanogens (Speece 1996; White 2000; Ecke and Lagerkvist, 2000; De Mes et al., 2003). Figure 1.1 summarizes the process. Organic matter can contain long chain polymers including particulate carbohydrates, lipids and proteins. The complex and insoluble polymer cannot penetrate cellular membranes and is not directly consumed by the microorganisms. The first step is called hydrolysis in which the complex organic matter is broken down into soluble organic matter (monomers) containing sugars, amino acids and fatty acids by hydrolytic bacteria. Subsequently, these soluble molecules are converted into fatty acids and alcohols by acidogenic bacteria/fermenting bacteria. During acetogenesis, acetogenic bacteria convert these fatty acids and alcohols into acetate and hydrogen and CO_2 . In the last step (methanogenesis), methanogens use acetic acid or CO_2 and hydrogen to produce CH_4 and CO_2 . In addition to the four main steps in the anaerobic digestion carbon flow (metabolic pathway), there is a linkage between acetic acid and hydrogen and CO_2 . Hydrogen and CO_2 may be converted to acetate by the homoacetogenic bacteria (White, 2000). On the other hand, acetate may be converted to hydrogen and CO_2 by acetate oxidizing organisms (Karakashev et al. 2006). Overall, anaerobic digestion carbon flow is a complex pathway (McMahon et al. 2004).

Anaerobic digestion process performance depends on operating parameters such as temperature, mixing, hydraulic retention time (HRT), solid retention time (SRT) as well as digester configuration. Digestion is often operated in the mesophilic range (30 to 38°C or 95 to 105°F). It is also possible to operate in the thermophilic range (50 to 57°C or 122 to 136°F (Metcalf and Eddy, 2003). Optimum pH for methanogenesis is in the range of 6.8–8.3 (Speece, 2008).

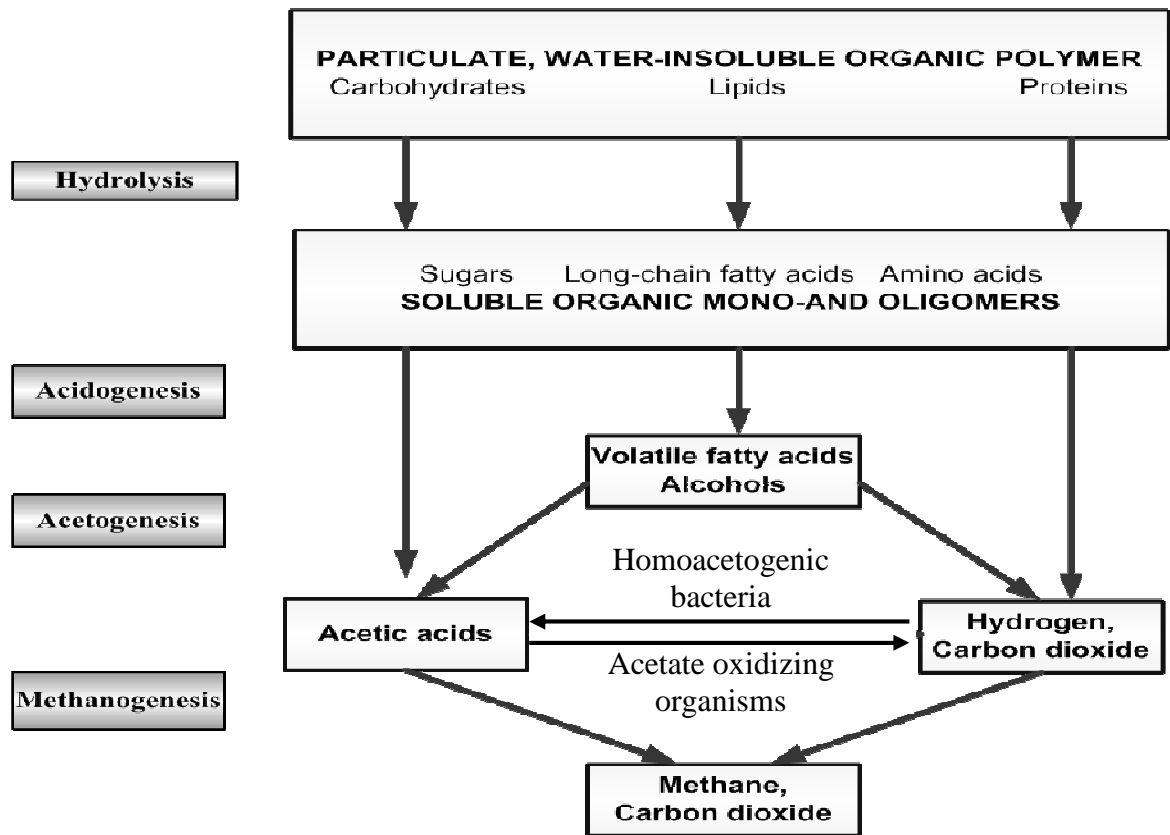


Figure 1.1: Summary of the anaerobic digestion carbon flow

For treating high strength organic pollution, anaerobic treatment is often more cost effective than aerobic treatment. Moreover, energy recovery from CH_4 produced, lower operating cost (no aeration required) and the capability of handling higher loading rates are benefits that encourage the use of anaerobic treatment as a sustainable treatment technique.

A modification called “co-digestion” is now used. In co-digestion, a mixture of waste/feedstocks from multiple locations is treated together (Ahring et. al., 1992). In this way, more organic carbon is added to make efficient use of existing digesters to produce more CH_4 . When various wastes are mixed and co-digested, synergistic, neutral and

antagonistic outcomes are possible. Before describing these outcomes, advantages and disadvantages of co-digestion are described below.

1.1.2 Advantages and disadvantage of anaerobic co-digestion

A significant opportunity exists to increase renewable energy production using existing anaerobic digesters. Use of co-digestion at municipal anaerobic digesters is typically focused on increasing sustainable waste treatment for communities, increased revenue and renewable energy production. Many municipal digesters exist and are distributed around the United States. For example, there are 1455 municipal wastewater treatment plants (including 104 plants with combined heat and power installations) in the United States and more than 60 municipal wastewater treatment plants in the state of Wisconsin that have anaerobic digesters (EPA, 2011; Vik, 2003). Furthermore, the biogas already produced is often used for renewable energy for combined heat and power (CHP) applications including electricity generation. Existing municipal digesters have excess capacity and could treat other co-digestates. When multiple co-digestates are properly blended, more organic carbon can be digested at a facility to produce more CH_4 and renewable energy.

Increased use of co-digestion can help reduce greenhouse gas (GHG) emissions. GHG emission from materials such as dairy manure that release CH_4 to the atmosphere can be reduced by collecting and burning the CH_4 . Also, the biogas can replace fossil-fuel-derived electricity that generates CO_2 from sequestered carbon, such as coal. It is estimated that biogas plants in Denmark reduced the country's total 1996 GHG emissions

by 0.3% (Maeng et al., 1999). Biomass carbon, such as that in food, ethanol and bio-diesel production waste, is primarily derived from CO₂ fixed from air; therefore digesting and burning this organic carbon recycles CO₂ back to the atmosphere with little or no net increase.

Other advantages of co-digestion are cost-sharing by processing multiple wastes in a single facility, equalization of floating, settling, acidifying wastes through dilution and improved nutrient balance. Others report the optimum C/N/P ratio (on a mass basis) to be 100-128/4/1 (Rizk et al., 2007). Chen et al. (2008) listed an optimum C/N ratio (on a mass basis) of 20 and COD/N ratio (on a mass basis) of 70. Some co-digestates may have a higher C/N ratio, meaning that available nitrogen may not be adequate, and it would be beneficial to add other co-digestates that have a low C/N ratio. In this way, co-digestion may improve digester performance through better nutrient balance. Moreover, co-digestion can be used to gain revenue such as carbon credits, tipping fees, and renewable energy tax credits in addition to revenue from biogas for electricity and heat. However, there are significant expenses such as transportation as well as digested biosolids handling and disposal costs. It is important to consider these revenue and expense items when selecting promising wastes for co-digestion.

1.1.3 Disadvantage of anaerobic co-digestion

There are a few disadvantages of full scale anaerobic co-digestion. Since each waste comes to a wastewater treatment plant from a different location, there could be high conveyance / transportation costs. In some locations, when waste conveyance is not

possible on a daily basis, a large tank for temporary storage of waste generated and received may be required. When waste has large particles, pretreatment may be required for size reduction before co-digestion. Moreover, when multiple wastes and variable feeds are digested together, there may be the possibility for foaming in the digester.

1.1.4 Synergism, antagonistic and neutral outcomes

Anaerobic co-digestion can result in different outcomes including synergism, antagonistic or neutral outcomes depending on waste identity and characteristics. These outcomes can be defined based upon CH_4 production that is greater than, less than or the same as that observed when each material is digested alone (Zitomer et al., 2008). Therefore, anaerobic co-digestion with synergistic waste is gaining increased attention. However, identification of synergistic wastes is challenging since co-digestion outcomes have not been studied for a broad range of wastes. Synergistic outcomes may occur when substrate utilization rate can be increased through optimum nutrient balance of blended wastes. Antagonistic outcomes may result from inhibitory concentrations of toxic substances in one or more wastes. However, other fundamental mechanisms for these outcomes have not been defined. It is important to develop a proper method for investigating these outcomes for engineering applications.

Successful combinations of different types of wastes and wastewater require careful management. Batch anaerobic bioassay techniques have been developed by others as simple and inexpensive procedures to monitor relative biodegradability and possible toxicity of wastes to be treated by anaerobic digestion. There are currently two

assay tests, (1) biochemical CH_4 potential (BMP) and (2) anaerobic toxicity assay (ATA), to identify potential co-digestates for anaerobic co-digestion. Also, these two tests can be used to determine synergistic, neutral and antagonistic outcomes as described in the subsequent part of this Chapter. The BMP and ATA tests are relatively simple bioassays that can be conducted in laboratories without the need for sophisticated equipment.

1.1.5 Biochemical methane potential (BMP) test

The BMP is a measure of sample biodegradability (Owen *et al.*, 1979). The BMP test is a screening tool to determine the CH_4 volume that can be produced from a waste's short-term, non-steady state digestion. In other words, the BMP is a measure of what fraction of a given wastes' COD can be converted to CH_4 anaerobically (Speece, 1996). The assay provides a simple means to monitor relative anaerobic biodegradability of substrates. Uses of the BMP are as follows:

- Assaying the concentration of organic pollutants in a wastewater which can be anaerobically converted to CH_4
- Evaluating potential anaerobic process efficiency
- Measuring residual organic pollution amenable to further anaerobic treatment
- Testing for non-biodegradable chemical oxygen demand (COD) remaining after treatment

1.1.6 Anaerobic toxicity assay (ATA) test

The ATA was developed to determine any toxic effect of a substance or waste on the organisms that convert acetate to CH_4 (Owen *et al.*, 1979). These organisms are

typically considered to be the microbes most sensitive to toxicants in the mixed microbial culture that achieves CH₄ production from complex substrates. Like the BMP test, the ATA test is relatively simple. The significant difference between the BMP and ATA assays is that the ATA is supplemented with a high concentration of acetate as well as varying wastewater concentrations, whereas no acetate is added to the BMP system. The ultimate or maximum biogas produced is most important in the BMP test, whereas the initial rate of gas production is of primary interest in the ATA test (Speece, 1996).

1.1.7 Economic analysis

BMP and ATA results can be used to help select the most promising wastes for bench-scale testing. However, these tools don't reveal the actual worth of co-digestion. Therefore net cost-benefit analysis should be performed by considering all estimated benefits and costs related to co-digestion. The benefits include revenue from biogas-generated electricity and heat, carbon credits, tipping fees, renewable energy tax credits and any other benefits that accrue. The costs include transportation and digested biosolids handling costs. It is important to consider all revenue and costs when selecting promising wastes for co-digestion.

1.1.8 Bench-scale anaerobic co-digestion

Most previous bench-scale co-digestion studies focused on optimizing process performance by determining blending ratio of co-digestates with municipal sludge. In addition, foaming potential and volatile solids destruction should be observed using bench scale testing before implementing full-scale co-digestion. Previous bench- and pilot-scale studies of co-digestion have been performed using various co-digestates.

Typical co-digestates combined with municipal sludge include fat, oil and grease (Kabouris et al., 2008; Kabouris et al., 2009), food waste (Kim et al., 2004; Di Palma et al., 1998; Bjornsson et al., 2000; Edelman et al., 2000; Lafitte-Toru and Forster, 2000), algae (Cecchi et al., 1996), winery wastewater (Rodriguez et al., 2007), confectionary waste including syrups (Lafitte-Toru and Forster, 2000), cattle manure, fruit and vegetable and poultry waste (Misi and Forster, 2002), slaughterhouse waste including stomach content and dissolved air floatation float (Rosenwinkel and Meyer, 1999), paper mill sludge and organic fraction of municipal solid waste (Einola et al., 2001), wood waste and starch hydrolyzate (Converti et al., 1997) and the organic fraction of municipal solid waste including office paper, newspaper, grass clipping and dog food production waste (Schmit and Ellis, 2001).

1.1.9 Full-scale-scale anaerobic co-digestion

There has been some full scale co-digestion testing and implementation conducted in the past two decades. Full-scale thermophilic anaerobic co-digestion of cow manure and oil or waste from protein extraction from bone was reported (Ahring et al., 1992). Fats, oils and grease (FOG) was co-digested with wastewater treatment plant sludge in Oxnard, CA (Alatrisme-Mondragon et al., 2006; Bailey, 2006); Lincoln, NE and East Bay Municipal Utilities District, CA (Schater et al., 2007); Redwood and Riverside, CA (Bailey, 2006); Milbrae, CA (Chung, 2007; York, 2009); Watsonville, CA (Cockrell, 2008); and South-Cross Bayou Water Reclamation Facility (WRF) and Pinellas County, FL (Kabouris et al., 2007, Kabouris et al., 2009). Most of the full-scale co-digestion studies for municipal anaerobic digesters were performed with addition of FOG. The

expansion of full-scale co-digestion to other possible co-digestates should be investigated.

1.1.10 Research hypothesis

In this study, three hypotheses were considered:

1. Co-digestion of some co-digestates increases biogas production significantly more than predicted by digestion of each co-digestate alone.
2. Co-digestion of some co-digestates increases specific methanogenic activities (SMAs) against acetate, propionate and hydrogen.
3. Co-digestion of acid whey in full-scale demonstrates a synergistic outcome (produces additional CH_4 greater than anticipated theoretical CH_4 from chemical oxygen demand (COD)).

1.2 Methodology

The work described herein was performed to assess anaerobic co-digestion of various wastes with municipal primary sludge as a sustainable energy technology. However, synthetic primary sludge was used for bench-scale testing to avoid the high variability of real primary sludge and potential infection from pathogens from real sludge. High-organic-strength wastes were considered from sources located within 100 miles (160 km) from South Shore Wastewater Reclamation Facility (SSWWRF) in Oak Creek, WI. After the most promising co-digestates were selected for possible full-scale digestion, the capability of the existing equipment at the wastewater treatment plant was considered.

This study focused on protocols of co-digestate selection for full-scale applications and increased renewable energy. The research work was divided into four parts: (1) identification of promising co-digestates using a market study, (2) identification of at least 5 promising co-digestates using waste characterization and simple economic analysis, (3) determination of performance of bench-scale co-digestion for selected co-digestates, and (4) determination of performance of full-scale co-digestion for one of the best co-digestates. The research plan is shown in Figure 1.2.

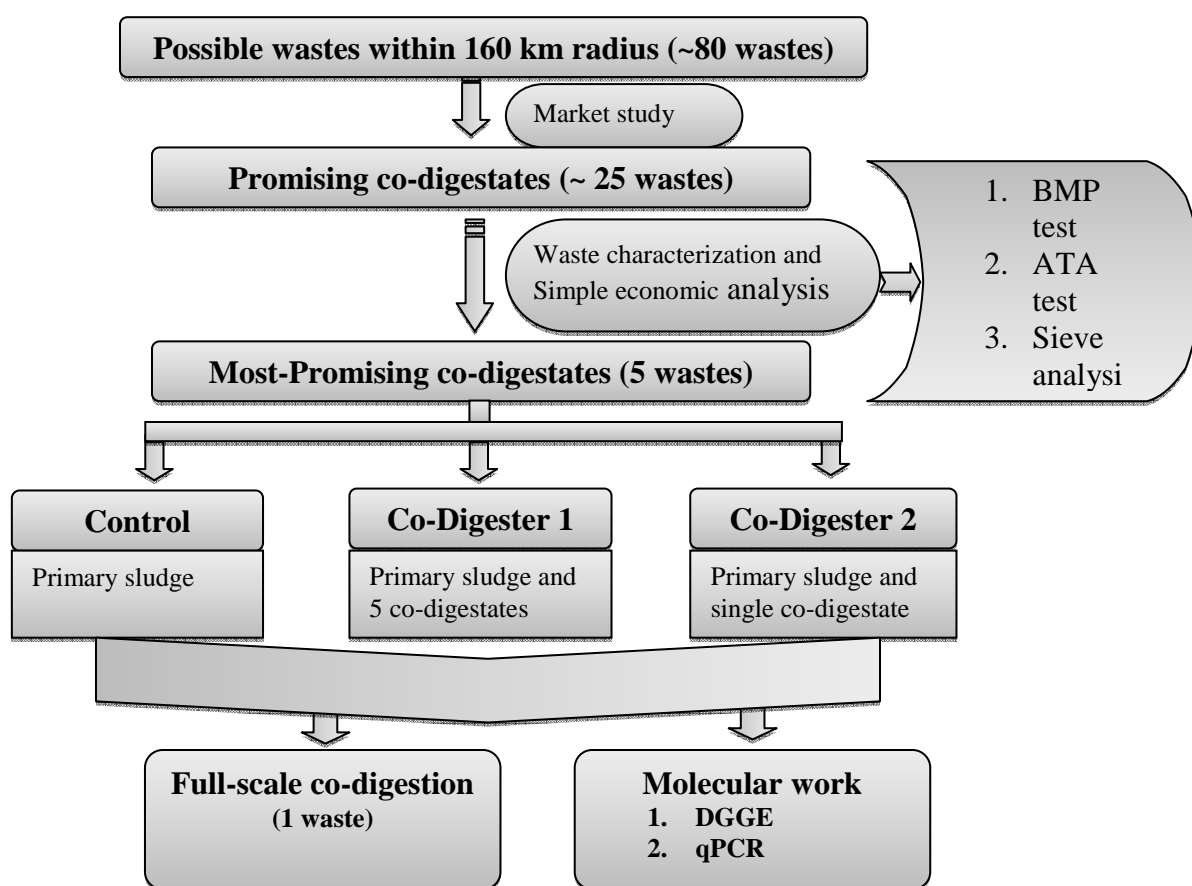


Figure 1.2: Research work plan schematic diagram

1.2.1 Preliminary screening

A market survey was performed primarily to identify high-strength wastes produced within a 160-km radius of the Milwaukee Metropolitan Sewerage District (MMSD) South Shore Wastewater Reclamation Facility (Oak Creek, WI, USA). However, the market study was extended to identify bio-refinery wastes even though the distance to the SSWWRF was more than 160 km. Industries were contacted and questioned using a questionnaire for assessment of potential feedstock to municipal anaerobic digesters. The questionnaire included questions about potential co-digestate identity, quantity and constituent concentrations. For simplicity, a facility contact person was requested to fill out a table which was comprised of the following details:

1. Facility waste stream
2. Facility name
3. Facility address
4. Facility contact person
5. Facility email address and phone number
6. Current disposal method (Landfill, wastewater treatment, land application)
7. Quantity (lb/day) or (gal/day)
8. Organic strength (mg/L VS, mg/L VSS, mg/L COD, mg/L BOD₅ other)

1.2.2 Identify most promising co-digestates

After preliminary screening, the promising wastes were sampled and characterized by constituent analyses, BMP, ATA and sieve analysis testing.

1.2.2.1 Biochemical methane potential (BMP) testing

The BMP protocol of Owen et al. (1979) was used as one of the tools to screen co-digestates in terms of the volume of CH_4 produced per unit of waste at 35°C and 1 atm. Seed biomass was used from a bench-scale anaerobic digester fed non-fat dry milk and nutrients. All systems were seeded with 30 mL of biomass. No basal media was added to all systems. Test assay and standard contained approximately 65 mg COD of waste or glucose, respectively, in addition to the biomass, and seed blanks received no waste (see Figure 1.3).

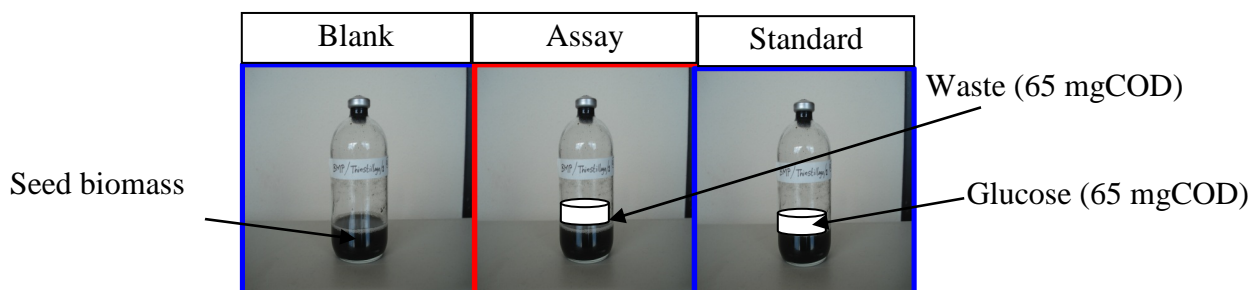


Figure 1.3: BMP experiment set-up

Testing was conducted in 160-mL serum bottles sparged with oxygen-free gas (7:3 v/v $\text{N}_2:\text{CO}_2$) and sealed with solid, black, butyl rubber stoppers and aluminum-crimped seals. All testing was performed in triplicate at 35°C and 150 rpm using an incubator shaker (model C25KC, New Brunswick Scientific, Edison, NJ). The biogas volume produced was measured at ambient pressure and 35°C every day using a 100-mL glass syringe with a wetted glass barrel. Syringe content was re-injected into the serum bottle after volume measurement. Headspace CH_4 content was measured by gas chromatography (GC). Net CH_4 production was calculated as the total volume of CH_4 produced by seed blanks subtracted from the total volume of CH_4 produced in test

systems. BMP was calculated as the net CH₄ production divided by the co-digestate COD or VS added to the serum bottle.

1.2.2.2 Anaerobic Toxicity Assay (ATA) testing

ATA tests were performed to determine the potential inhibitory or stimulatory affect of each waste on maximum CH₄ production rate from acetate (Owen et al., 1979). For each assay, different doses of waste (< 12 g COD/L) were added along with calcium acetate (10 g/L) as the main, non-limiting substrate to 50 mL of biomass. Seed biomass was used from a bench-scale anaerobic digester fed non-fat dry milk and nutrients. Testing was conducted in 160-mL serum bottles sparged with oxygen-free gas (7:3 v/v N₂:CO₂) and sealed with solid, black, butyl rubber stoppers aluminum-crimped seals. All testing was performed in triplicate at 35°C and 150 rpm using an incubator shaker (model C25KC, New Brunswick Scientific, Edison, NJ). The biogas volume produced was measured at ambient pressure and temperature of 35°C every day using a 100-mL glass syringe with a wetted glass barrel. The maximum CH₄ production rate was determined by linear regression using the initial portion of a graph of cumulative CH₄ production versus time. A dose-response curve was prepared by plotting the maximum CH₄ production rate versus waste dose. For inhibitory wastes, the concentration causing a 50% decrease in CH₄ production rate (IC₅₀ concentration) was determined from a graph of CH₄ production rate versus waste dose.

1.2.2.3 Sieve analysis

There was a concern that large solid particles in the waste could potentially damage pumps and other equipment and settle in the unmixed waste storage tank and the digester at the treatment plant. Therefore it was important to determine particle size distribution of each waste. This test was performed using a standard sieve analysis method. For sieve analysis, sieves with minimum opening size of 0.053mm (No 270) and maximum opening size of 4.75mm (No 4) were used. In this test, each waste was allowed to pass through the selected, stacked sieves. The number of sieves used in these tests was in the range of 4 to 6 because 4 sieves were enough for some wastes in which most of the particles (> 99%) passed through all the sieves. The total dry mass of retained particles on each sieve was measured. Percent (%) retained and % passing were also calculated. Finally, a plot of % passing versus sieve opening size was constructed for each waste (i.e., a “sieve curve”). The d_{10} (sieve opening size passing 10% of the material), d_{50} and d_{90} were calculated from the plots.

1.2.2.4 Analytical methods

Chemical oxygen demand (COD), soluble chemical oxygen demand (SCOD), total solids (TS), volatile solids (VS), ammonia nitrogen ($\text{NH}_3\text{-N}$), total Kjeldahl nitrogen (TKN), total phosphorous and alkalinity concentrations were measured using standard methods (APHA et al., 1998). Fats, oils and grease (FOG) was measured using EPA (1999). The pH was measured using a glass electrode and meter. Biogas CH_4 content and volatile fatty acid (VFA) concentrations were determined by gas chromatography (Series 7890A GC system, Agilent Technologies, Santa Clara, CA,

USA) with a thermal conductivity detector (TCD) and flame ionization detector (FID), respectively. In waste characterization, total phosphorus, $\text{NH}_3\text{-N}$, TKN and FOG were analyzed by Mike Dollhopf, Lab Manager of the Water Quality Center, Marquette University.

1.2.2.5 Metals analyses

The samples were sent to Northern Lake Service, Inc., 400 North Lake, Crandon, WI for metals analyses. The methods for digesting samples for metals analysis are presented in Table 1.1. Methods of digestion were different for solid/semi-solid samples and liquid samples. The brewery grain, paunch, dried manure, float, flavorings yeast, yeast centrate, sprout, wet distillers grain, syrup, whole stillage, thin stillage, waste rice, waste noodles, mustard, metal cutting fluids waste, oil and hydraulic fluids, packaging waste and white waste were in the solid/semisolid waste category. The acid whey, brewery yeast, trube, cookie waste, soap, confectionary waste, boiler cleaning waste and can crushing waste were in the liquid waste category.

Table 1.1: Analysis methods for solid/semisolid and liquid samples

Metals	Digestion via		Instruments
	Solid/semisolid	Liquid	
Arsenic v	SW846 7060	SM 3113-B 19ed	GFAA
Cadmium, Chromium, Copper, Lead, Molybdenum, Nickel, Potassium, Silver, Zinc	SW846 6010	EPA 200.7	ICP-MS, Agilent 7700
Mercury	SW846 7470A	EPA 245.1	Cold Vapor
Selenium	SW846 7740	SM 3113-B 19ed	GFAA

GFAA: Graphite Furnace Atomic Absorption Spectrophotometry

ICP-MS: Inductively Coupled Plasma-Mass Spectroscopy

SW846: Test Methods for Evaluating Solid Waste Physical/Chemical Methods published by Environmental Protection Agency (EPA)

SM 3113: Standard Method for metal analysis in water and wastewater published by EPA

1.2.2.6 Economic analysis

A simple cost-benefit analysis was performed for co-digestates. The estimated net worth of each co-digestate was calculated as the sum of the estimated value of CH₄ produced (0.21 United State Dollar (USD)/m³CH₄ @ 35°C), GHG avoided (0.003 USD/kg CO₂) and treatment charges (0.28 USD/kg COD and 0.28 USD/kg TSS) less the sum of waste conveyance (0.16 USD/m³-km) and solids handling and disposal (0.110 USD/dry TS kg). The CO₂ avoidance was estimated assuming fuel switching from bituminous coal (emission factor = 0.088 kg CO₂/ MJ). The emission factor for bio CH₄ was assumed to be negligible since the CO₂ emitted was assumed to be originally fixed from the atmosphere. The unit GHG emission credit value was estimated from the average daily closing price of 2003-vintage CO₂ credits on the Chicago Climate Exchange. Unit treatment fees were estimated based on current municipal waste treatment fees charged by municipalities in and near Milwaukee, Wisconsin. The waste BOD₅ concentration was estimated to be 50% of the measured COD concentration. Waste conveyance unit cost was estimated from tanker truck contract costs after discussion with regional trucking companies. Solids handling and disposal unit cost (E) was estimated after discussion with operators of various wastewater treatment plants. A volatile solids reduction value of 50% was assumed; therefore, solids to be disposed of were assumed to be composed of half of the waste volatile solids and all of the inert solids. A CH₄ heat content (G) of 35 MJ/m³ CH₄ at 35°C was employed. Subsequently, the selected most promising wastes were co-digested in the bench-scale digesters.

1.2.3 Performance of bench-scale anaerobic digesters

Performance of co-digestion was investigated using pairs of bench-scale digesters under three conditions (Control, Co-Digester 1 and Co-Digester 2) based on biogas production, percent CH₄ content, total and individual VFA and TS and VS destruction. In addition, foaming potential and any synergistic outcome were also observed as an indicator of digester performance.

1.2.3.1 Anaerobic digester set-up

Six laboratory-scale anaerobic digesters were fabricated using a transparent acrylic cylinder of 14-cm internal diameter and 30-cm height. Both ends were sealed by an acrylic plate. Each digester had an approximate total volume of 4.5 L and working liquid volume of 2.5 L. Magnetic mixing was provided to achieve completely mixing in the digester. Each digester was provided with three ports: one for feeding the sludge, a second for withdrawal of digested biosolids, and one for biogas collection. The biogas generated during digestion was collected in a 10-L polyvinyl fluoride film (PVF) gas sampling bag. A schematic diagram of the bench-scale anaerobic digesters is given in Figure 1.4.

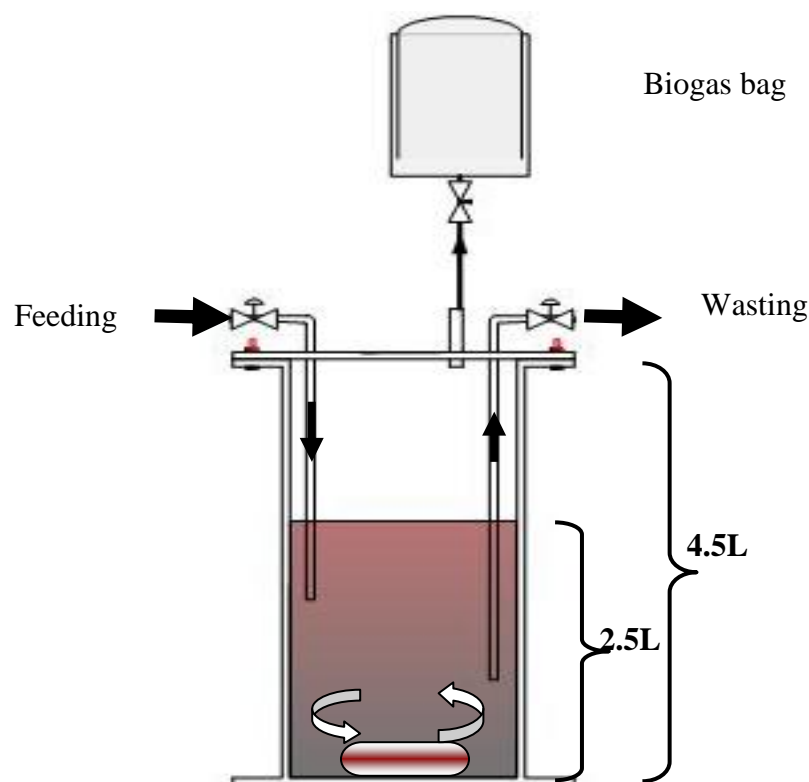


Figure 1.4: Schematic diagram of bench-scale anaerobic digester

1.2.3.2 Digester start-up and operation

All digesters (R1, R2, R3, R4, R5, and R6) were initially seeded with biomass from a full-scale anaerobic digester at SSWRF. Right after inoculation, headspace in the digesters was sparged with oxygen-free gas containing 30% CO₂/70% N₂. The digesters were kept under continuously mixed condition using magnetic stirrers (150 rpm) in a temperature-controlled room (35°C). During the first two days, digesters were kept without feeding. However, biogas production and pH were monitored. Digesters were operated with daily wasting and feeding (semi-continuous mode) at a solids retention time (SRT) of 15 days. Synthetic primary sludge (TS = 2.9% and VS = 2.4%) contained a mixture of organic (12% fat, 26% protein 5% fiber) and inorganic solids

(Natural Choice Dog Food, NutroProducts, Inc., City of Industry, CA, USA) and anaerobic basal medium (see Table 1.2).

Table 1.2: Basal medium

	Concentration (mg/L)
NH ₄ Cl	400
MgSO ₄	250
KCl	400
CaCl ₂	120
(NH ₄) ₂ HPO ₄	80
FeCl ₃ .6H ₂ O	55
CoCl ₂ .6H ₂ O	10
KI	10
Metals*	0.5
Alkalinity	5000
*Metals include MnCl ₂ .4H ₂ O, NH ₄ VO ₃ , CuCl ₂ .2H ₂ O, Zn(C ₂ H ₃ O ₂) ₂ .2H ₂ O, AlCl ₃ .6H ₂ O, NaMoO ₄ .2H ₂ O, H ₃ BO ₃ , NiCl ₂ .6H ₂ O, NaWO ₄ .2H ₂ O and Na ₂ SeO ₃ added together to make a 0.5mg/L metals solution.	

The volume of biogas produced was measured by forcing the collected biogas through a wet test gas meter (every two days after wasting and feeding). The Control (R1 and R2), Co-Digester 1(R3 and R4), and Co-Digester 2(R5 and R6) systems were fed with synthetic primary sludge for the first 55 days (>3 SRTs).

After Day 55, Co-Digester 1 systems were fed with a mix of 5 of the most promising co-digestates in addition to synthetic primary sludge. Co-Digester 2 systems were fed with synthetic primary sludge and the most promising co-digestate. After Day 55, co-digester 1 systems (R3 and R4) were fed the following five most promising co-digestates (described in Table 1.6), which were identified through simple economic analysis, in addition to synthetic primary sludge: float (3.1 mL/d, 0.52 gCOD/d), can

crushing waste (2.8 mL/d, 0.22 gCOD/d), thin stillage (4.9 mL/d, 0.76 gCOD/d), flavorings yeast (1 mL/d, 0.26 gCOD/d), and acid whey (3.7 mL/d, 0.54 gCOD/d). Co-Digester 2 systems (R5 and R6) were fed with synthetic primary sludge and flavorings yeast waste (4 mL/d, 1.05 gCOD/d) which was shown to have synergistic affects in previous work (Zitomer et al., 2008). Control systems were continuously fed with only synthetic primary sludge. The loading rates of individual co-digestates to bench-scale anaerobic digesters were selected based on the actual full-scale co-digestate volumes produced and the full-scale digester volume at the SSWWRF. This loading ratio may or may not be optimum. The analytical frequency of parameters is presented in Table 1.3.

Table 1.3: Analysis parameters in anaerobic digestion

Parameter	Frequency
Biogas production	1/2days
Biogas composition	2/week
Individual and total VFA	2/week
Soluble chemical oxygen demand (SCOD)*	2/week
pH*	7/week
Alkalinity	2/week
TS*	2/week
VS*	2/week

*- parameters were also measured for each feed.

All digesters were operated until quasi-steady state was reached. The quasi steady state was reached either when the effluent characteristics did not vary more than 10% or after 3 SRTs of operation time (i.e., 45 days). After quasi-steady state, NH_3 , TKN, total suspended solids (TSS), volatile suspended solids (VSS), and total soluble organic carbon (TOC) concentrations were measured using standard methods (APHA et al., 1998) for at least 5 measurements.

1.2.4 Specific methanogenic activity

The digester performance or "activity" of microbial cultures was determined using SMA tests of biomass samples against acetate, propionate and H₂ according to standard methods (Angelidaki et al. (2007) for acetate and propionate; Coates et al. (2005) and Coates et al. (1996) for H₂).

Assays were conducted in triplicate at 35°C, 150 rpm using an incubator shaker (model C25KC, New Brunswick Scientific, Edison, NJ). All assays were performed under anaerobic conditions in 160-ml serum bottles. The VS concentration of the biomass was measured at the beginning of activity tests.

1.2.4.1 SMA against acetate and propionate

Fifteen mL (140-180 mg VS) and 25 mL (240-300 mgVS) of biomass were used in acetate and propionate activity tests, respectively. The final total volume of the assay was kept at 30 mL by adding the appropriate amount of basal media. Bottles were sparged with oxygen-free gas (7:3 v/v N₂:CO₂), closed with solid, black, butyl rubber septa and incubated. Approximately 3 days were allowed for degassing from residual COD in the biomass. CH₄ content in the headspace was measured using gas chromatography (GC). Substrates were injected through the septum using a syringe and needle to achieve a calcium acetate concentration of 12 g/L and a calcium propionate concentration of 3.4 g/L. The biogas volume produced was measured at ambient pressure and 35°C every day using a 10- or 100-mL (depending upon gas production) glass syringe with a wetted glass barrel. The syringe content was re-injected into the serum

bottle after volume measurement. Headspace CH_4 content was measured by GC at the end of testing.

For acetate and propionate activities, maximum CH_4 production rate ($\text{mL CH}_4/\text{day}$) was determined by linear regression of the initial, linear portion of a plot of cumulative CH_4 production versus time. SMA values ($\text{mL CH}_4/\text{g VS-day}$) were calculated by dividing maximum CH_4 production rate values by average VS mass.

1.2.4.2 SMA against H_2

A sample of 8 to 12 mg VS of biomass was used in hydrogenotrophic activity tests. The final total volume of the assay was kept at 30 mL by adding the appropriate amount of basal media. Bottles were sparged with oxygen-free gas (7:3 v/v $\text{N}_2:\text{CO}_2$), closed with solid, black, butyl rubber septa and incubated. Then, 3 days were allowed for degassing from residual COD in the biomass. Subsequently, 100 mL of an H_2 and CO_2 gas mixture (at a ratio of 1:4, v/v) at ambient pressure and temperature was injected through the septum using a syringe and needle; then the bottles were incubated. Bottle headspace volume was measured by inserting the needle of a glass syringe with wetted barrel at ambient pressure and at 35°C twice a day for 7 days. Syringe content was re-injected into the serum bottle after volume measurements.

For hydrogenotrophic activity, the volume of $\text{H}_2:\text{CO}_2$ gas utilized was calculated as from the decrease in the gas volumes in the assay plus the gas volume produced from endogenous control bottles at the given period of time. CH_4 production was estimated as

the volume of $\text{H}_2\text{:CO}_2$ gas utilized divided by 4 based upon the stoichiometry of CH_4 production from H_2 and CO_2 (1 mol CH_4 produced from every 4 mols H_2 and 1 mol of CH_4). Maximum CH_4 production rate ($\text{mL CH}_4/\text{day}$) was determined by linear regression of the initial, linear portion of a plot of cumulative CH_4 production versus time. SMA values ($\text{mL CH}_4/\text{g VS-day}$) were calculated by dividing maximum CH_4 production rate values by average VS mass.

1.2.5 Co-Digestion with synergistic, antagonistic and neutral outcomes

A series of BMP tests (13 tests) were performed to determine if co-digestion of different combinations of selected wastes resulted in synergistic, antagonistic or neutral outcomes. The most promising wastes (5 wastes) which were co-digested in the bench-scale Co-Digester 1 systems and one of the antagonistic wastes (metal cutting fluid) were used for BMP testing with synthetic primary sludge. BMP testing was conducted for each waste alone and together with synthetic primary sludge (1:1 COD basis). All BMP tests were conducted using the procedure described in Section 1.2.2.1.

1.2.6 Full-Scale co-digestion testing at SSWWRF

The most promising waste (acid whey) was co-digested with municipal wastewater sludge (primary sludge) in five operating anaerobic digestion tanks (named D6, D8, D10, D11 and D12) at the SSWWRF. The total volume of the five tanks was 12 million gallons (MG). Tanks D6 and D8 were 1.5 MG each, whereas tanks D10, D11 and D12 were 3MG each. The waste was transported using tanker trucks that could contain a

maximum of 5500 gallons based on transportation weight limits, then stored in an existing 80,000 L tank at the treatment plant and pumped using a metering pump (model 23H1-K20Z-2131, Chemtron, Inc.) to the feed line to all of the digesters. A maximum of 27,500 gallons (5 truckloads) per week of the acid whey was fed at an average rate of 10.2 liters per minute over 61 days. Digester stability/operations, volatile solids removal and CH₄ production during co-digestion were compared to those observed during a previous 60-day period when only wastewater sludge was digested (control period) and a 50-day period from the time when acid whey feeding was stopped (post co-digestion period). The primary sludge fed to the digesters was combination of primary sludge from the Jones Island Wastewater Reclamation Facility (JIPS) and SSWERF primary sludge (SSPS). A schematic diagram of feed and waste streams at SSWWRF is given in Figure 1.5.

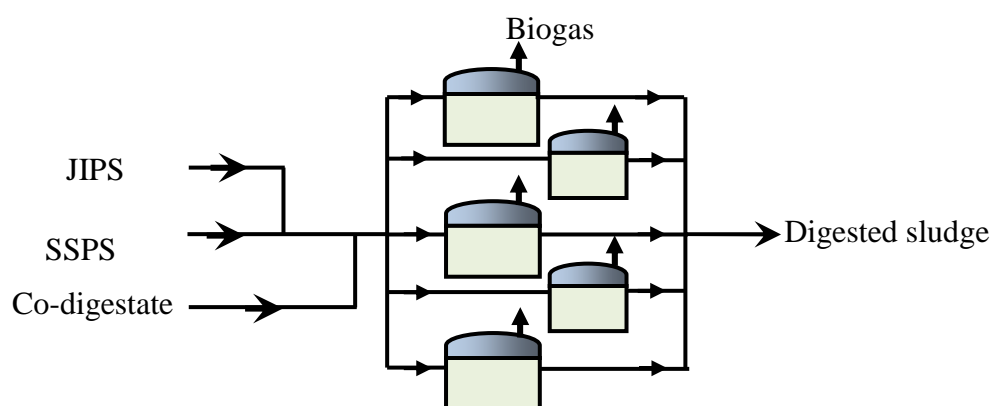


Figure 1.5: Feed and waste streams at the SSWWRF

1.2.6.1 Sampling and analysis

Sampling frequency and parameters analyzed are listed in Table 1.4. Samples for COD, NH₃-N and TKN analysis were preserved by H₂SO₄ immediately after samples were collected. Total daily biogas volume (summed value) from all five digesters was measured using exiting gas meters. CH₄ content of biogas was measured once a week.

Table 1.4: Testing schedule during co-digestion^{1,2,3}

Parameters	JISS	SSPS	Digested sludge	Co-digestate	Frequency
Flow rate	X	X	X	X	daily
Duration of flow	X	X	X	X	daily
pH	X	X	X**	X	daily
TS	X	X	X	X	1/week
VS	X	X	X	X	1/week
Total VFA	X	X	X**	X	1/week
COD	-	-	X	X*	2/week
NH ₃ -N	-	-	X	X*	2/week
TKN	-	-	X	X*	2/week
Alkalinity	-	-	X**	-	1/week
Temperature	-	-	X**	-	daily

X = measurement/analysis was performed

¹ All samples are weekly composite sample unless otherwise noted

² * two grab samples

³ ** measured for each digester separately

The operational conditions during three periods (Control, Co-Digestion and Post Co-Digestion) are presented in Table 1.5. The average COD of acid whey was 59300 ± 7400 mg/L.

Table 1.5: Operational conditions of digesters

Paramerters	Control	Co-Digestion	Post Co-Digestion
SRT (days)	22	20	22
Average primary sludge loading rate (gTS/L-day)	1.25	1.48	1.23
Average primary sludge loading rate (gVS/L-day)	0.92	0.99	0.95
Average acid whey flow rate (L/min)	0	10.21	0
Average acid whey loading rate (g COD /L-day)	0	0.019	0

1.2.6.2 Mass balance

A mass balance of VS for the full-scale anaerobic digesters was calculated. This mass balance was used to calculate the CH₄ yield per unit mass of VS destroyed.

1.2.7 Statistical analyses

All statistical analyses were performed using ANOVA standard software (Statistics 18, SPSS Inc., Chicago, IL USA).

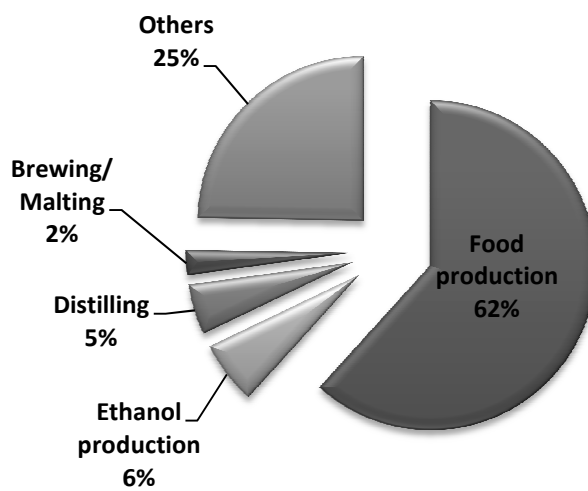
1.3 Results and Discussion

The results and discussion of this chapter are described under the following subsections: market study; identify most promising co-digestates; performance of bench-scale co-digesters; specific methanogenic activities; synergistic, antagonistic and neutral outcomes; and performance of full-scale co-digesters.

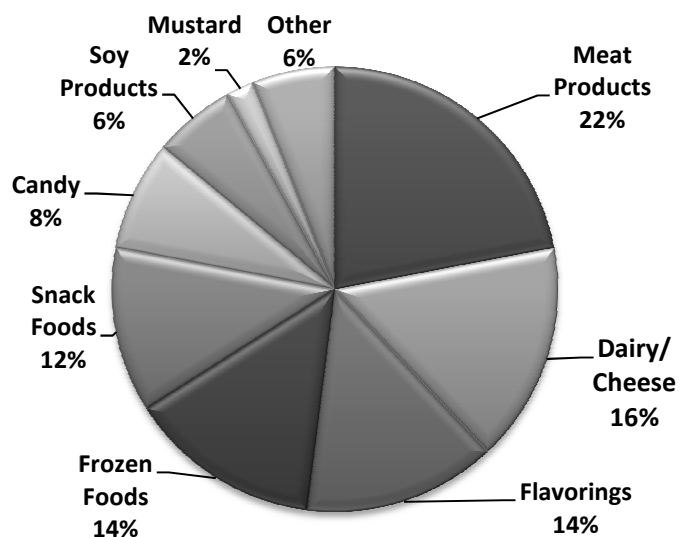
1.3.1 Market study

There were 81 wastes from 54 facilities identified during the market survey. The sources of wastes are presented in Figure 1.6. Other wastes included algae removed from

lakefront areas, zoo animal waste, and soap production wastes. More than 50% of wastes were identified as food production wastes (see Figure 1.6 a). The main food production wastes were meat products, flavorings, frozen foods, dairy/cheese and snack foods (see Figure 1.6 b). The maximum distance between the source of each waste and SSWWRF was 16 km for 20% of wastes, 48 km for 39% of wastes, 80 km for 52% wastes and 160 km for 100 % of wastes. However, one of wastes, Fischer-Tropsch (FT) reactor condensate waste, was identified as an interest even though it was at a distance of 1500 km. This was included since it is of special interest as a biorefinery waste..



(a) All wastes tested



(b) Food production waste tested

Figure 1.6: Sources of wastes identified for co-digestion

1.3.2 Identify most promising co-digestates

From preliminary screening, 46 wastes (see Table 1.6) were chosen for characterization based upon the significant volume produced, high COD concentration, and/or proximity to the digester.

Table 1.6: Waste characteristics and facility descriptions for potential co-digestates

Waste	COD (mg/L or other as marked)	TS (%)	Description	Distance to digester, km
Cooking solids	1,056,000*	46.8	Meat Production	10
Wood chip/Charcoal	660,000*	39.6		
Flavorings yeast	216,000	15.7	Food flavorings production	12
Yeast centrate	35,000	0.6		
Sprout	127,000*	14.3		
Oil and hydraulic fluids	77,000	2.6	Metal recycling facility	20
Compost	174,000*	56.8	Garden waste (Plant wastes, grass, clippings and cocoa husks)	21
Cocoa husks	350,000*	64.1		
Alage (Botrycoccus braunii)	1,749,000*	98.7	Liquid bio-fuel from algae	24
Alage (Nannochloropsis)	1,413,000*	96.8		
Lettuce	50,000*	7.0	Vegetable food production	24
Pine apple	94,000*	4.1		
Potatoes waste	126,000*	14.7		
Cabbage waste	50,000*	4.8		
Heads from rum distillation	1,444,000	0.0	Rum distillation	25
Molasses wash	126,000	9.3	Rum fermentation	
Corn/Rye/Wheat/Barley in liquid	172,000	11.9	Distillation	
Float	133,000*	12.5	Dissolved air flotation float from meat production	26
Paunch	105,000*	10.6	Meat production	
Dried manure	449,000*	86.4		
Pre-filter slurry	39,000	11.9	Shave gel production	26
Trube	203,000	9.9	Beer fermentation	29
Brewery yeast	313,000	16.2		
Brewery grain	107,000	20.1		

* These values are in units of mg/kg (wet)

Table 1.6: Waste characteristics and facility descriptions for potential co-digestates (continued)

Waste	COD (mg/L or other as marked)	TS	Description ¹	Distance to digester, km
Soap	47,000	2.0	Soap production	29
Corrugated cardboard	1,184,000*	92.6	N/K	30
Boiler cleaning waste	33,000	5.7	Coal-fired boiler heat exchanger cleaning solution	48
Metal cutting waste	75,000	2.3	Machine shop	48
Mustard waste	59,000*	8.5	Mustard production	53
Sorghum	89,000	5.6	Winery production	56
Packaging waste	972,000*	76.8	Waste candy from packaging operation	71
White waste	1,089,000*	90.1	Floor sweepings from candy production	71
Acid whey	148,000	12.7	Soft cheese production	79
Confectionary	23,000	1.9	Candy production	89
Waste rice	287,000*	22.7	Frozen food production	98
Waste noodle	502,000*	35.3		
Cheese waste	438,000*	72.1	Cheese production	106
Wet distillers grain	206,000*	31.1	Corn ethanol production	110
Syrup	399,000	30.4		
Whole stillage	155,000	14.5		
Thin stillage	137,000	9.1		
Can crushing waste	76,000	6.1	Soft drink production	120
Cookie waste	13,000	0.6	Industrial bakery	153
Dewatered paper mill sludge	311,000*	35.6	Paper/tissue production	156
Corn Stover	1,662,000*	90.3	Corn Production	160
FT reactor condensate	104,000	0.0	Liquid bio-fuel from wood	1535

* These values are in units of mg/kg (wet)

¹ N/K: Not known

1.3.2.1 Constituent analyses

Summary of waste constituent analyses for 46 wastes which were chosen from the market study are presented in Table 1.7. These constituent analyses included pH, TS, VS, TSS, VSS, COD, total phosphorous, $\text{NH}_3\text{-N}$, TKN, FOG, alkalinity and selected metals in each waste. The selected metals analyses included heavy metals: cadmium, chromium, lead, arsenic, mercury, trace metals: copper, selenium, nickel, zinc, molybdenum and light metals: potassium and silver. Based on the metals analysis, trube, brewing yeast, acid whey and soap waste contained high potassium concentrations (540, 2300, 3300 and 900 mg/L, respectively). Boiler cleaning waste contained significant amounts of copper (68 mg/L) and chromium (6.9 mg/L). The FOG concentrations of waste are presented in Table 1.7. High FOG was observed in float waste (59400 mg/kg of wet sample) and in syrup (51640 mg/L).

Table 1.7: Summary of waste characteristics

	1	2	3	4	5	6	7
Parameters	Trube	Brewing yeast	Grain	Cookie	Soap	Packaging	White waste
pH	4.02	4.88	3.9	4.79	12.26	-	-
TS (%)	9.9	16.2	21.4	0.6	2	89.1	91.1
VS (%)	9.5	14.3	20.1	0.5	1.2	76.8	90.1
TSS (mg/L)	33933	138200	-	3330	59	-	-
VSS (mg/L)	33133	129333	-	2997	40	-	-
COD (mg/L)	203,294	313,380	107377*	12,543	47,299	972 083*	1089391*
Total Phosphorus (mg/L)	248	1,509	3973*	19	87	86.3*	400*
NH3-N (mg/L)	50	218	66*	0	137	0.7*	0.06*
TKN (mg/L)	2,828	24,724	41698*	51	241	45.7*	3.67*
FOG (mg/L)	4,580	280	N/A	3,309	4,837	18*	21
Alkalinity (mg/L as CaCO3)	0	35.7	0	34.8	4994	-	-
BMP (mlCH4/gCOD or mlCH4/gVS)	373 ± 15	373 ± 6	367 ± 8	418 ± 19	< 20	301 ± 12	306 ± 9
ATA	IC50=1.8%	IC50=4.7%	IC50>10%	IC50>50%	IC50=2%	IC50>1%	IC50>1%
d _{10%} Passing (mm)	< 0.053	< 0.053	< 0.053	< 0.053	< 0.053	> 4.75	< 0.71
d _{50%} Passing (mm)	< 0.053	< 0.053	1.17	0.2	< 0.053	> 4.75	> 4.75
d _{90%} Passing (mm)	0.12	< 0.053	> 2.0	0.53	< 0.053	> 4.75	> 4.75
Cadmium (ug/L)	3.2	12	<0.40*	4.4	1.7	0.01*	0.017*
Chromium (ug/L)	13	80	<0.53*	13	17	0.05*	0.068*
Copper (ug/L)	7300	5000	20*	370	86	0.8*	0.8*
Lead (ug/L)	<13	<13	<5.6*	29	<13	0.11*	<0.052*
Nickel (ug/L)	22	22	1.2*	18	<12	<0.03*	<0.052*
Zinc (ug/L)	2700	9000	78*	520	50000	26*	1.76*
Arsenic (ug/L)	<2.4	<2.4	<3.7*	5.9	<2.4	<0.34*	<0.48*
Selenium (ug/L)	15	<31	8.2*	<3.1	<3.1	<0.43*	<0.6*
Silver (ug/L)	<12	<12	<0.36*	<1.2	<12	<0.034*	<0.048*
Molybdenum (ug/L)	510	370	3*	<3.3	<33	<0.09*	<0.132*
Potassium (ug/L)	540,000	2,300,000	0.017%DWB	21,000	900,000	94*	216*
Mercury (ug/L)	<4.9	<27	<0.064*	<4.8	<49	<0.001*	<0.006*
Quantity (gal/day or lb/day)	750gpd	10000gpd	N/A	600gpd	10000gpd	N/A	40000lb/day

* - Unit: mg/Kg of sample

Table 1.7: Summary of waste characteristics (continued)

	8	9	10	11	12	13	14
Parameters	Confectionary	Float	Paunch	Manure	Flavorings yeast	Yeast centrate	Sprout
pH	6.1	5.5	7.29	-	5.4	4.96	5.75
TS (%)	1.9	12.53	13.04	92.86	15.71	0.59	15.00
VS (%)	1.8	11.31	10.56	86.42	15.09	0.57	14.33
TSS (mg/L)	33232	-	-	-	168333	1127	-
VSS (mg/L)	29277	-	-	-	330444	1260	-
COD (mg/L)	23,150	132816*	104847*	449369*	215,599	35,479	127243*
Total Phosphorus (mg/L)	31	5179*	8223*	2163*	1,123	67	4403*
NH3-N (mg/L)	<0.03	3967*	920*	414*	112	11	1968*
TKN (mg/L)	7	41752*	19522*	2768*	10,904	801	53522*
FOG (mg/L)	933	59400*	N/A	N/A	2,530	4,465	N/A
Alkalinity (mg/L as CaCO3)	242.6	-	-	-			-
BMP (mlCH4/gCOD or mlCH4/gVS)	346 ± 14	416 ± 19	<u>237 ± 20</u>	<u>51 ± 8</u>	326 ± 34	285 ± 6	<u>389 ± 13</u>
ATA	IC50>40%	IC50>10%	IC50>10%	IC50>3%	IC50>5%	IC50>30%	IC50>10%
d _{10%} Passing (mm)	< 0.053	< 0.075	< 0.71	< 0.71	< 0.053	< 0.053	< 0.053
d _{50%} Passing (mm)	< 0.053	< 0.075	1.1	2.26	< 0.053	< 0.053	> 0.25
d _{90%} Passing (mm)	< 0.053	0.52	> 4.76	> 4.76	< 0.053	< 0.053	> 0.25
Cadmium (ug/L)	7	<0.49*	<0.39*	<0.28*	<0.17*	<2.9*	<0.34*
Chromium (ug/L)	59	11*	<0.52*	2.9*	<0.25*>	<3.9*	<0.45*
Copper (ug/L)	600	31*	22*	11*	11*	56*	9.7*
Lead (ug/L)	<13	<6.9*	<5.6*	<4.0*	<2.4*	<41*	<4.8*
Nickel (ug/L)	41	6.6*	1.9*	2.1*	2.3*	<6.2*	<2.5*>
Zinc (ug/L)	1700	200*	85*	<2.5*	560*	<6.4*>	69*
Arsenic (ug/L)	<12	<4.2*	<3.8*	<2.5*	<1.7*	<27*	<3.2*
Selenium (ug/L)	<15	<5.2*	<4.8*	<3.1*	<2.1*	<34*	<0.4*
Silver (ug/L)	<12	<0.44*	<0.36*	<0.025*	<0.15*	<2.6*	<0.3*
Molybdenum (ug/L)	<33	1.5*	1.2*	0.77*	<3.0*	<8.3*>	<1.1*>
Potassium (ug/L)	14000	0.079%DWB	0.39%DWB	0.43%DWB	0.21%DWB	0.74%DWB	0.93%DWB
Mercury (ug/L)	<0.05	<0.095*	<0.17*	<0.083*	<0.067*	<0.54*	<0.08*
Quantity (gal/day or lb/day)	275gpd	10000gpd	50000gpd	N/A	192000lb/wk	108000lb/wk	3000gpd

* - Unit: mg/Kg of sample

Table 1.7: Summary of waste characteristics (continued)

	15	16	17	18	19	20	21
Parameters	Wet distill. grain	Syrup	Whole stillage	Thin stillage	Waste rice	Waste noodle	Acid whey
pH	3.65	3.52	3.51	3.61	3.30	4.38	4.51
TS (%)	32.94	30.44	14.45	9.12	22.98	36.21	12.70
VS (%)	31.14	27.44	13.49	8.27	22.69	35.29	10.75
TSS (mg/L)	-	-	-	-	-	-	221
VSS (mg/L)	-	-	-	-	-	-	189
COD (mg/L)	206243*	398,718	154,778	137,241	286867*	502416*	147,990
Total Phosphorus (mg/L)	15179*	9,996	3,067	1,395	124.3*	382.5*	1,595
NH3-N (mg/L)	400*	246	34	42	158.3*	131.5*	272
TKN (mg/L)	24775*	2,722	9,447	3,086	2490*	4332*	848
FOG (mg/L)	N/A	51,640	N/A	31,370	N/A	N/A	748
Alkalinity (mg/L as CaCO3)	-	-	-	-	-	-	0
BMP (mlCH4/gCOD or mlCH4/gVS)	<u>473 ± 15</u>	396 ± 22	399 ± 7	351 ± 14	<u>414 ± 21</u>	<u>453 ± 10</u>	295 ± 3
ATA	IC50>6%	IC50>4%	IC50>10%	IC50>12%	IC50>6%	IC50>3%	IC50>8%
d _{10%} Passing (mm)	< 0.075	< 0.053	< 0.075	< 0.075	> 4.75	> 4.75	< 0.053
d _{50%} Passing (mm)	0.47	< 0.053	0.39	< 0.075	> 4.75	> 4.75	< 0.053
d _{90%} Passing (mm)	1.46	< 0.053	> 0.71	< 0.075	> 4.75	> 4.75	< 0.053
Cadmium (ug/L)	<0.16*	<0.18*	<0.17*	<0.28*	<0.25*	<0.16*	<1.8>
Chromium (ug/L)	<0.29*>	<0.35*>	<0.24*>	<0.47>	<0.33*	<0.72*>	53
Copper (ug/L)	3.9*	4.2*	4.1*	4.1*	2.2*	2.8*	<6.7
Lead (ug/L)	<2.3*	<2.5*	<2.5*	<3.9*	<3.6*	<2.3*	<6.5
Nickel (ug/L)	2.0*	2.9*	3.1*	3.2*	<1.7*>	2.0*	<6.0
Zinc (ug/L)	44*	80*	51*	83*	15*	14*	3300
Arsenic (ug/L)	<1.5*	<1.6*	<1.7*	<2.8*	<2.2*	<1.5*	<120
Selenium (ug/L)	<1.8*	<2.0*	<2.1*	<3.5*	<2.7*	<1.8*	<15
Silver (ug/L)	<0.14*	<0.16*	<0.16*	<0.25*	<0.23*	<0.15*	<6.0
Molybdenum (ug/L)	<0.74*>	<0.43*>	<0.53*>	<0.77*>	<0.48*	<0.31*	<3.3
Potassium (ug/L)	0.98%DWB	2.1%DWB	1.2%DWB	2.1%DWB	0.029WB	0.086%DWB	3300000
Mercury (ug/L)	<0.09*	<0.054*	<0.066*	<0.051*	<0.078*	<0.035*	<0.25
Quantity (gal/day or lb/day)	N/A	86000gpd	680000gpd	430000gpd	N/A	N/A	N/A

* - Unit: mg/Kg of sample

Table 1.7: Summary of waste characteristics (continued)

	22	23	24	25	26	27	28
Parameters	Boiler cleaning	Mustard waste	Metal Cutting	Oil and hydraulic fluids	Can crushing waste	Sorghum	Heads from rum distillation
pH	9.32	3.42	9.40	5.59	3.30-3.35	4.58	6.66
TS (%)	5.75	9.21	2.29	2.60	6.76	5.57	0.00
VS (%)	4.80	8.53	2.23	2.37	6.72	4.78	0.00
TSS (mg/L)	873	64600	276	353	235	5513	12
VSS (mg/L)	713	63600	273	271	234	5307	7
COD (mg/L)	32,906	58,698*	75,351	76,875	81,749	89038	1443595
Total Phosphorus (mg/L)	79	914	123	22	50	272	1.98
NH3-N (mg/L)	-	43	133	395	3	17.4	ND
TKN (mg/L)	-	4,259	1,085	672	27	1410	210
FOG (mg/L)	-	5,320	32,150	7,350	416	380	50
Alkalinity (mg/L as CaCO3)	5710	0	2720	1365	0	243	8
BMP (mlCH4/gCOD or mlCH4/gVS)	< 20	580 ± 25	65 ± 8	79 ± 4	320 ± 15	260 ± 9	368 ± 12
ATA	IC50 = 9.5 %	IC50 = 14.4%	IC50 = 12.5%	IC50>15%	IC50>15%	> 12%	> 0.8%
d10% Passing (mm)	< 0.053	< 0.149	< 0.053	< 0.053	< 0.053	< 0.053	< 0.053
d50% Passing (mm)	< 0.053	1.27	< 0.053	< 0.053	< 0.053	< 0.053	< 0.053
d90% Passing (mm)	< 0.053	> 2.0	< 0.053	< 0.053	< 0.053	< 0.053	< 0.053
Cadmium (ug/L)	120	<0.024*>	<0.021*	<0.71*	<0.44>	1.7	<0.85
Chromium (ug/L)	6900	0.21*	<0.040*>	<3.1*>	44	23	<0.5
Copper (ug/L)	68000	0.87*	5.2*	170*	35	18000	23
Lead (ug/L)	<450	3.7*	3.7*	120*	<6.9>	18	<0.5
Nickel (ug/L)	18000	0.34*	<0.13*>	22*	31	83	<3.7
Zinc (ug/L)	6600	5.4*	5.4*	650*	380	1100	64
Arsenic (ug/L)	740	<0.17*	<0.18*	<7.0*	58	7.5	<6.5
Selenium (ug/L)	<580	<0.21*	<0.23*	<8.8*	47	<12	<12
Silver (ug/L)	<60	<0.018*	<0.019*	<0.64*	<1.4>	<1.1	<1.1
Molybdenum (ug/L)	-	<0.038*	<0.040*	11*	<9.0>	31	<3.8
Potassium (ug/L)	-	0.018%WWB	0.0018%WWB	0.19%DWB	34	2600	<0.75
Mercury (ug/L)	-	<0.0048*	<0.0051	<0.18*	0.59	0.31	0.22
Quantity (gal/day or lb/day)	ND	ND	ND	ND	ND	9 gpd	17 gpd

* - Unit: mg/Kg of sample

Table 1.7: Summary of waste characteristics (continued)

	29	30	31	32	33	34
Parameters	Molasses wash	Lettuce	Pine apple	Pre-filter slurry	Corn/Rye/Wheat/Barley in liquid	Corrugated Cardboard
pH	4.2	3.75	3.97	6.25	3.96	-
TS (%)	9.33	6.97	4.07	1.67	11.93	92.57
VS (%)	6.47	6.52	3.66	1.54	11.65	89.83
TSS (mg/L)	6733	-	-	-	-	-
VSS (mg/L)	5747	-	-	-	-	-
COD (mg/L)	125661	49554*	94061*	38555	171856	1184432*
Total Phosphorus (mg/L)	329	215*	50*	7.2	312	179*
NH3-N (mg/L)	37.5	93*	43*	202	19.9	34*
TKN (mg/L)	1720	1230*	820*	370	2540	832*
FOG (mg/L)	3300	325*	5822*	710	ND	8*
Alkalinity (mg/L as CaCO3)	0	0	0	-	-	-
BMP (mlCH4/gCOD or mlCH4/gVS)	251 ± 14	328 ± 22	516 ± 21	352 ± 23	326 ± 11	347 ± 20
ATA	> 8%	25%	> 15%	> 30%	> 8%	1.1%
d10% Passing (mm)	< 0.053	N/A	N/A	-	0	N/A
d50% Passing (mm)	< 0.053	N/A	N/A	-	-	N/A
d90% Passing (mm)	< 0.053	N/A	N/A	-	-	N/A
Cadmium (ug/L)	5.8	0.09	0.38	<1.3	62.8	0.13
Chromium (ug/L)	240	0.47	1.33	<30>	298	3.59
Copper (ug/L)	17000	8.42	15.29	84	8212	59.5
Lead (ug/L)	520	1.57	1.01	<13	1340	7.6
Nickel (ug/L)	370	2.3	9.5	<18	34560	28
Zinc (ug/L)	2000	6.4	9.8	160	9640	71.9
Arsenic (ug/L)	<7.5	0.04	0.05	7.3	12.8	ND
Selenium (ug/L)	<12	0.06	0	<12	111	5.8
Silver (ug/L)	13	13.9	17.4	<14	13820	161
Molybdenum (ug/L)	350	0.09	0.07	<10	225	2.97
Potassium (ug/L)	8900	1340	1600	220	739000	566
Mercury (ug/L)	<0.25	0.25	0.3	ND	202	1.65
Quantity (gal/day or lb/day)	17 gpd	100000 lbs/wk	100000 lbs/wk	10000 gpd	17 gpd	20 yd3 /week

* - Unit: mg/Kg of sample

Table 1.7: Summary of waste characteristics (continued)

	35	36	37	38	39	40	41
Parameters	FT reactor condensate	Cheese waste	Cooking solids	Wood chip/Charcoal	Dewatered paper mill sludge	Compost	Cocoa husks
pH	3.25	-	-	-	-	-	-
TS (%)	0.01	72.09	46.76	39.56	35.55	56.76	64.10
VS (%)	0.01	68.01	44.63	37.85	16.96	16.19	27.21
TSS (mg/L)	12	-	-	-	-	-	-
VSS (mg/L)	8	-	-	-	-	-	-
COD (mg/L)	103646	438005*	1056489*	659947*	311115*	174092*	350149*
Total Phosphorus (mg/L)	0.8	4615*	1189	561	78.8	474	1735
NH3-N (mg/L)	ND	6313*	343	10.9	0.4	140	4.9
TKN (mg/L)	ND	35640*	17094	181	0.5	4423	1022
FOG (mg/L)	ND	272000	650	210	ND	450	595
Alkalinity (mg/L as CaCO3)	-	N/A	N/A	N/A	N/A	N/A	N/A
BMP (mlCH4/gCOD or mlCH4/gVS)	365 ± 14	241 ± 28	366 ± 6	60 ± 11	254 ± 32	39 ± 6	49 ± 11
ATA	> 12%	> 3%	> 1%	> 1.6%	> 3%	> 6%	> 3%
d10% Passing (mm)	< 0.053	N/A	N/A	N/A	N/A	N/A	N/A
d50% Passing (mm)	< 0.053	N/A	N/A	N/A	N/A	N/A	N/A
d90% Passing (mm)	< 0.053	N/A	N/A	N/A	N/A	N/A	N/A
Cadmium (ug/L)	0.16	ND	0.13	0.05	0.46	0.83	0.02
Chromium (ug/L)	7.39	4.99	4.36	2.47	13.79	54.7	1.28
Copper (ug/L)	198	9.15	76.9	15.8	91	100	26.6
Lead (ug/L)	15.2	3	5.8	1.8	25.8	25.9	0.17
Nickel (ug/L)	14.2	2.45	9.93	1.52	11.7	11.9	0.53
Zinc (ug/L)	113	63.2	174	78.7	255	85.3	4.54
Arsenic (ug/L)	ND	ND	ND	ND	ND	1.45	ND
Selenium (ug/L)	0	0.34	ND	0.22	3	2.1	0.03
Silver (ug/L)	244	44.6	46.6	19.7	99.8	36	1.19
Molybdenum (ug/L)	27	0.19	0.26	0.09	0.94	0.41	ND
Potassium (ug/L)	491	764	114	1570	301	1900	57.6
Mercury (ug/L)	1.99	0.33	0.2	0.02	0.11	ND	ND
Quantity (gal/day or lb/day)	570 gpd	10-50 lbs/days	2150 lbs/day	270 lbs/day	400,000 lbs/day	10 yd3/month	ND

* - Unit: mg/Kg of sample

Table 1.7: Summary of waste characteristics (continued)

	42	43	44	45	46
Parameters	Potatoes waste	Cabbage waste	Corn Stover	Alage (<i>Botryococcus braunii</i>)	Alage (<i>Nannochloropsis</i>)
pH	-	-	-	-	-
TS (%)	14.74	4.76	90.30	98.67	96.81
VS (%)	13.89	4.34	80.76	91.52	87.71
TSS (mg/L)	-	-	-	-	-
VSS (mg/L)	-	-	-	-	-
COD (mg/L)	125952*	49957*	1662265*	1749000*	1413000*
Total Phosphorus (mg/L)	9.2	145	538000	-	-
NH ₃ -N (mg/L)	425	90.3	45400	-	-
TKN (mg/L)	2483	1153	602600	-	-
FOG (mg/L)	220	155	110	-	-
Alkalinity (mg/L as CaCO ₃)	N/A	N/A	N/A	-	-
BMP (mlCH ₄ /gCOD or mlCH ₄ /gVS)	282 ± 13	412 ± 4	396 ± 2	500 ± 27	394 ± 10
ATA	> 10%	> 25%	> 0.8%	> 0.8%	> 0.8%
d10% Passing (mm)	N/A	N/A	N/A	-	-
d50% Passing (mm)	N/A	N/A	N/A	-	-
d90% Passing (mm)	N/A	N/A	N/A	-	-
Cadmium (ug/L)	ND	ND	0.9	-	-
Chromium (ug/L)	ND	ND	19.2	-	-
Copper (ug/L)	8.9	5.1	146	-	-
Lead (ug/L)	ND	ND	24	-	-
Nickel (ug/L)	1.87	ND	15.7	-	-
Zinc (ug/L)	9.91	4.71	244	-	-
Arsenic (ug/L)	ND	ND	ND	-	-
Selenium (ug/L)	ND	ND	0.72	-	-
Silver (ug/L)	7.63	6.11	147	-	-
Molybdenum (ug/L)	ND	ND	0.44	-	-
Potassium (ug/L)	4060	1730	17200	-	-
Mercury (ug/L)	ND	ND	0.98	-	-
Quantity (gal/day or lb/day)	ND	ND	ND	300 yd ³ /Summer	300 yd ³ /month

* - Unit: mg/Kg of sample

1.3.2.2 Biochemical methane potential (BMP) testing

The BMP results for the 46 wastes are presented in Figure 1.7 a and b with units of mL CH₄/g COD and mL CH₄/gVS. CH₄ produced from all the co-digestates tested, with average BMP values (for 3 replicates) ranging from 20 to 418 mL CH₄/g COD and 39 to 580 mL CH₄/gVS. The BMP values of cookie and float wastes were slightly more than theoretical BMP value of 400 mL CH₄/g COD at 35°C. This may be due to experimental error or that the CH₄ produced in the seed sludge in the blank was less than that in the assay. High BMP values (>370 mL CH₄/gCOD) were observed for seven of the wastes: (1) cookie waste, (2) float, (3) whole stillage, (4) syrup, (5) trube (6) brewery yeast, and (7) mustard waste (see Figure 1.7 and 1.8). Low BMP values (< 100 mL CH₄/gCOD) were observed for oil and hydraulic fluids, metal cutting, soap, boiler cleaning, wood chip/charcoal, dried manure, cocoa husks and compost wastes (Figure 1.7 a and b). The average BMP result of glucose standards was 322 ± 23 mL CH₄/gCOD (a total of 21 glucose standard assays were run).

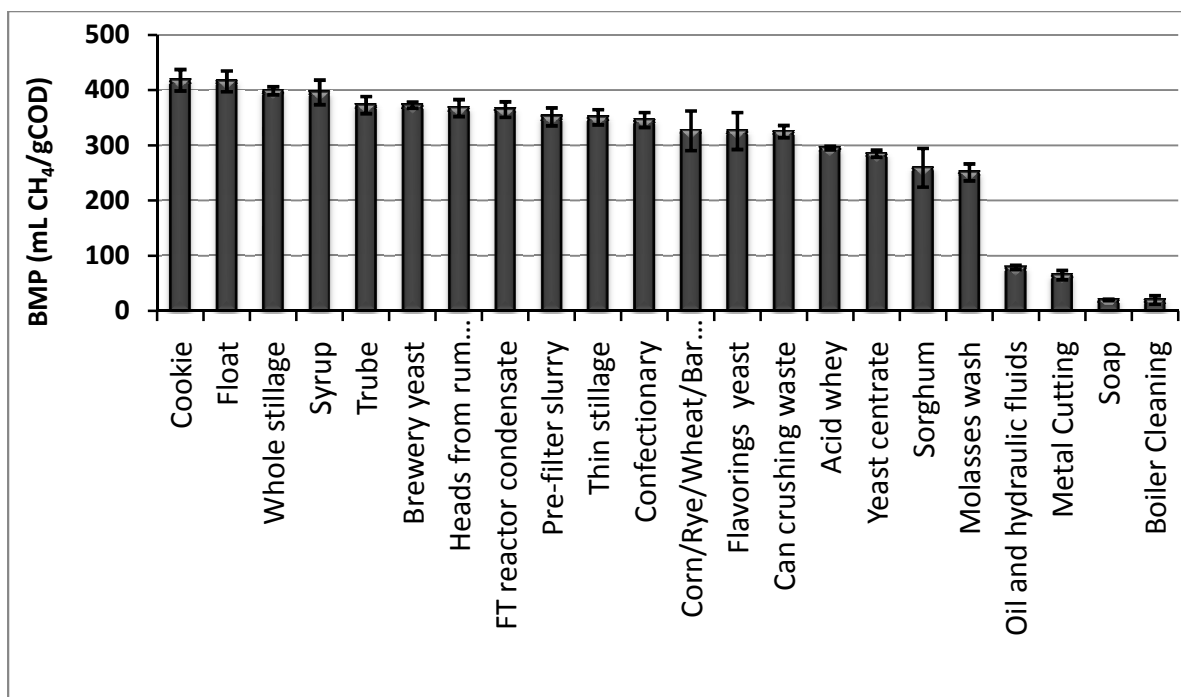


Figure 1.7(a): Biochemical methane potential (BMP) results for 22 promising co-digestates
 Error bars represent standard deviation of triplicate measurements. The CH₄ volume is reported at 35°C , 1 atm. Some error bars are too small to be visible.

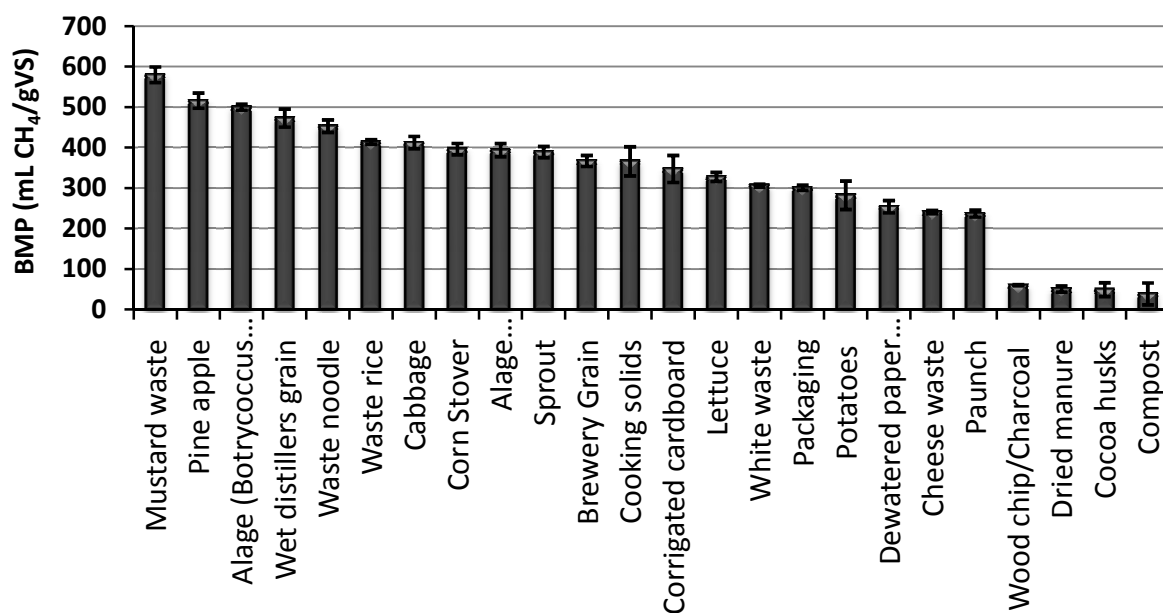


Figure 1.8(b): Biochemical methane potential (BMP) results for 24 promising co-digestates
 Error bars represent standard deviation of triplicate measurements. The CH₄ volume is reported at 35°C , 1 atm. Some error bars are too small to be visible.

1.3.2.3 Anaerobic toxicity assay (ATA) testing

The ATA results for various wastes include synergistic, antagonistic, neutral and mixed outcomes based on a comparison of maximum CH_4 production rates when calcium acetate was the main co-digestate in ATA testing (see Figures 1.9 through 1.12). ATA results of each outcome are shown in figures grouped by the range of doses to help present results more legibly. Whole stillage, thin stillage, can crushing waste, confectionary, yeast centrate, sorghum, potatoes waste, sprout, wet distillers grain, cheese waste, waste noodle, waste rice, syrup, molasses wash, packaging waste and white waste resulted synergistic outcomes (see Figure 1.9 (a), (b) and (c)). The maximum rate of CH_4 production increased more than 50% for whole stillage, packaging, white wastes and more than 30% for yeast centrate, syrup wastes, wet distillers grain and waste noodle. Sorghum, molasses and waste rice had more pronounced affects, increasing CH_4 production rate by approximately 90%.

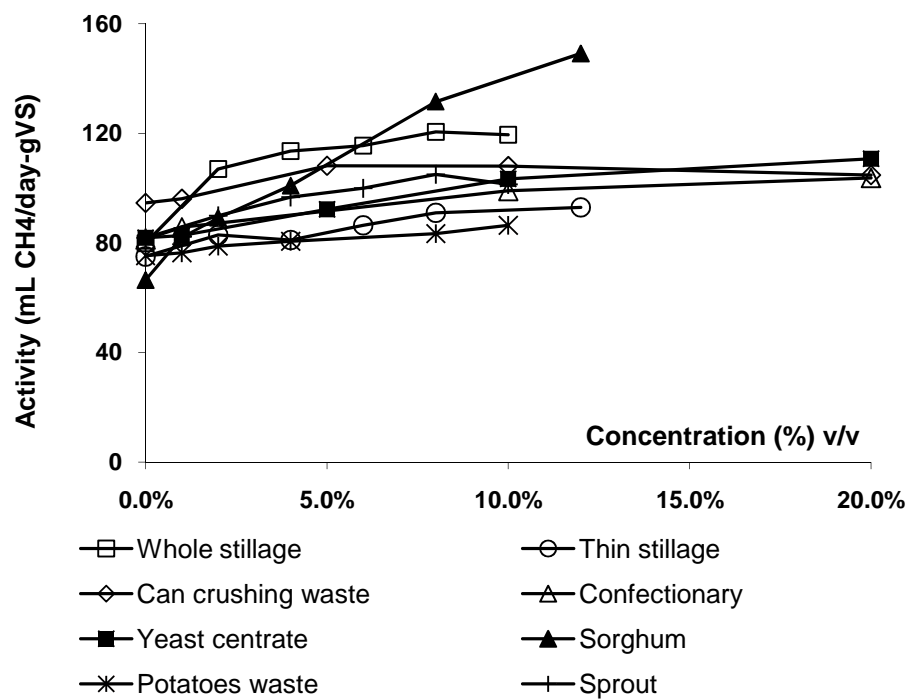


Figure 1.9: (a) Synergistic outcomes

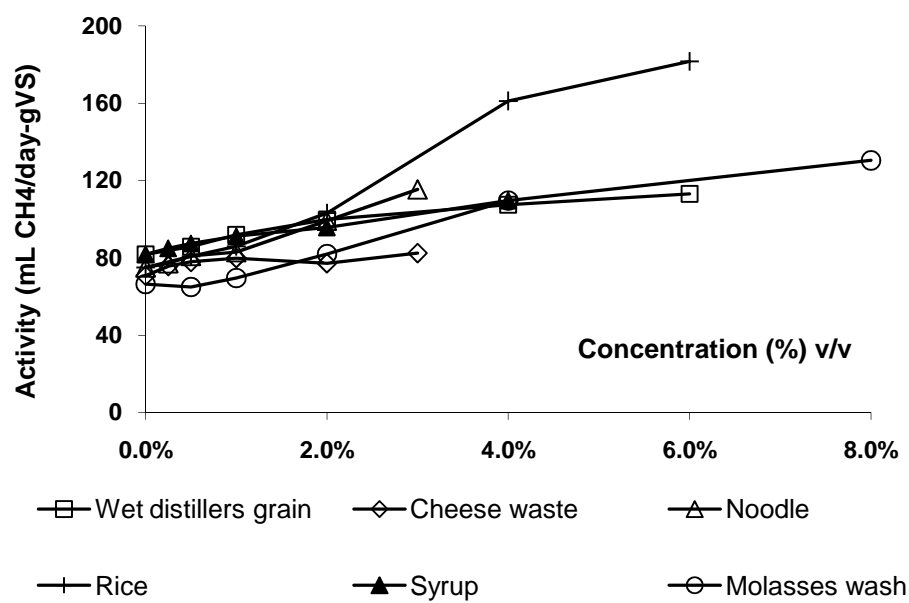


Figure 1.9: (b) Synergistic outcomes

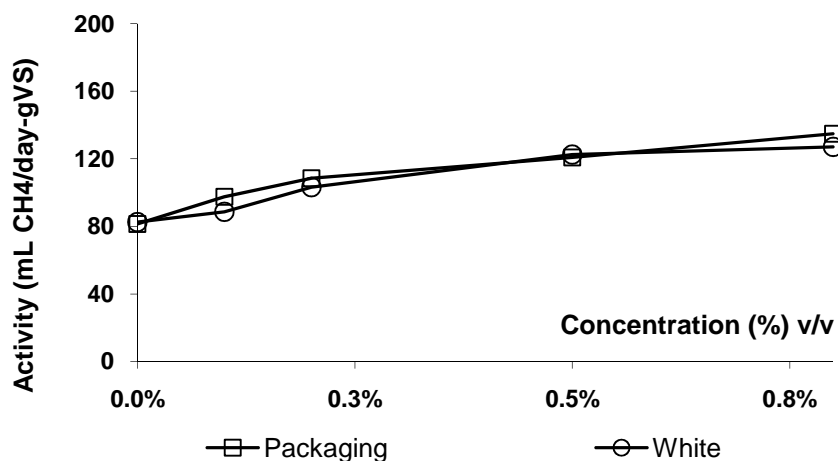


Figure 1.9: (c) Synergistic outcomes

Antagonism was observed for soap waste ($IC_{50} = 2\%$), boiler cleaning wastewater ($IC_{50} = 9.5\%$), metal cutting waste ($IC_{50} = 12\%$), oil and hydraulic fluids waste ($IC_{50} > 15\%$), cookie waste ($IC_{50} > 50\%$), lettuce waste ($IC_{50} = 25\%$), cabbage waste ($IC_{50} > 25\%$), mustard waste ($IC_{50} = 14.4\%$), compost ($IC_{50} > 6\%$), corrugated cardboard ($IC_{50} = 1.1\%$) and dried manure ($IC_{50} > 3\%$) (see Figure 1.10 (a) and (b)). Antagonistic outcomes may have been caused by inhibitory concentrations of zinc (50 mg/L) in soap and copper (68 mg/L), zinc (18mg/L) and chromium (6.9 mg/L) in boiler cleaning waste. The inhibitory substances in other wastes are unknown.

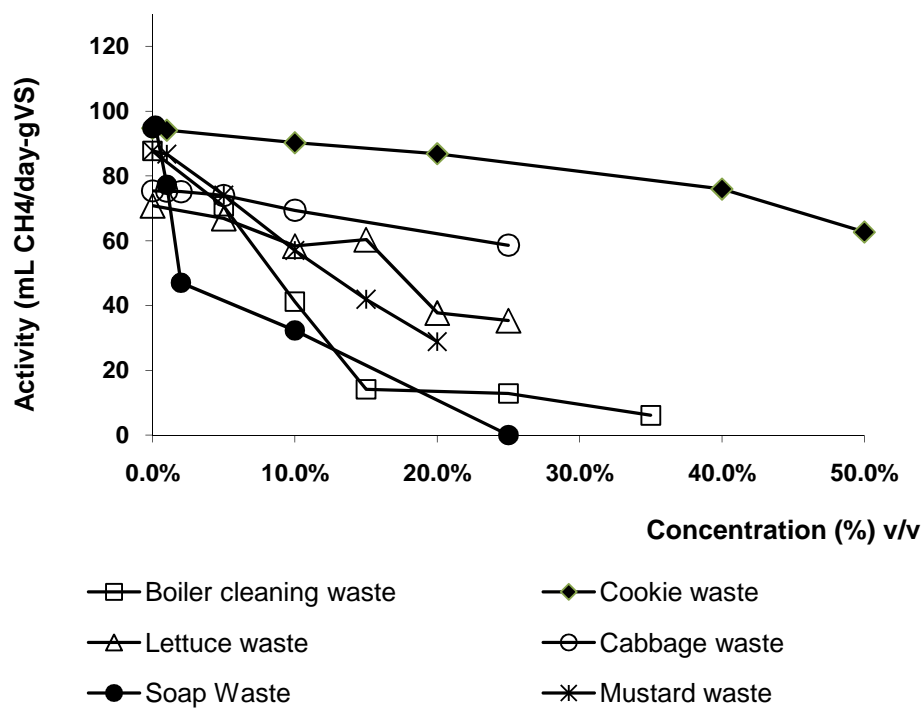


Figure 1.10: (a) Antagonistic outcomes

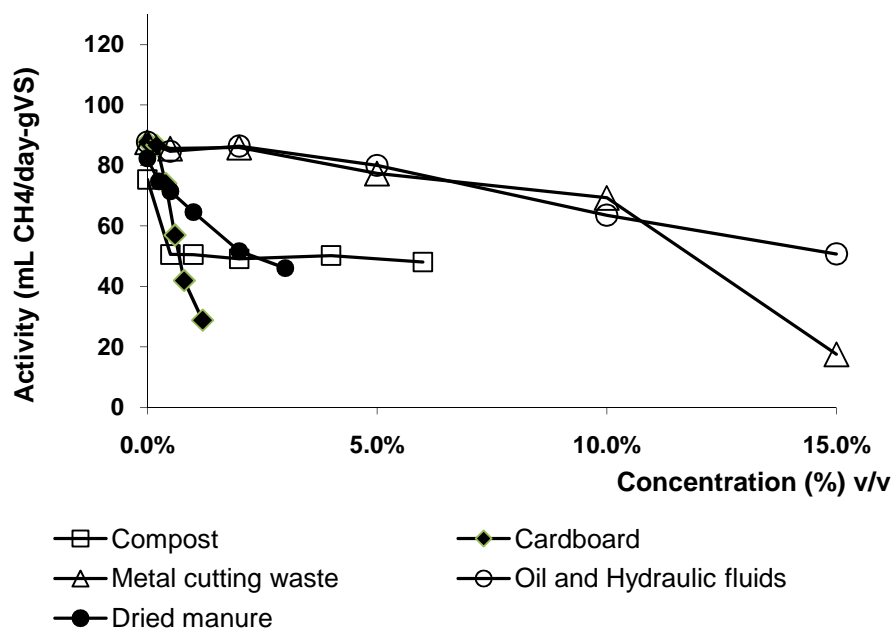


Figure 1.10: (b) Antagonistic outcomes

Neutral outcomes were observed for float, acid whey, paunch, brewery grain, algae (*botryococcus braunii*), algae (*nannochloropsis*), heads from rum distillation, cooking solids, wood chip/charcoal, corn stover, dewatered paper mill sludge, cocoa husks and pre-filter slurry (see Figure 1.11 (a), (b), and (c)). However, acid whey resulted in a synergetic outcome in subsequent studies (BMP test with synthetic primary sludge and full-scale test with primary sludge) which is described later in this chapter.

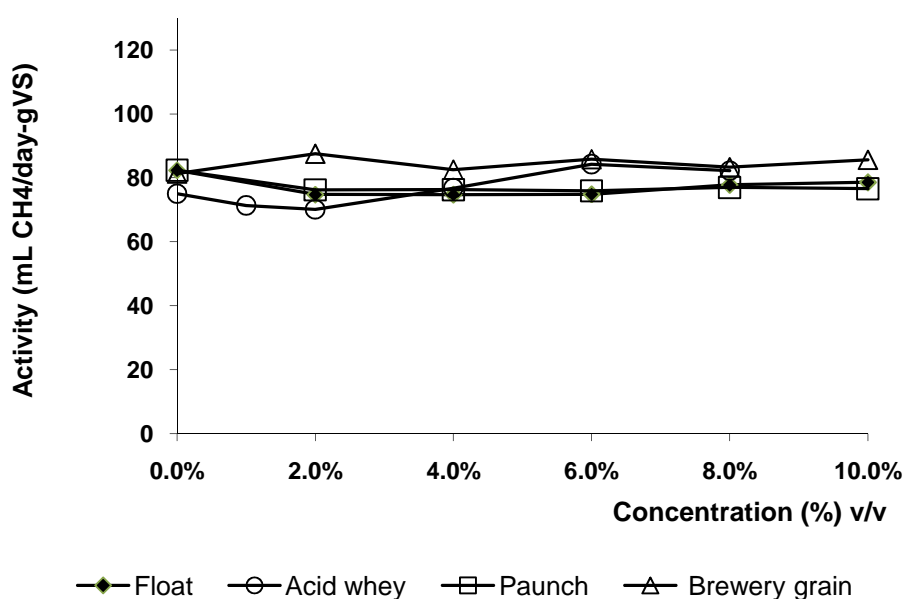


Figure 1.11: (a) Neutral outcomes

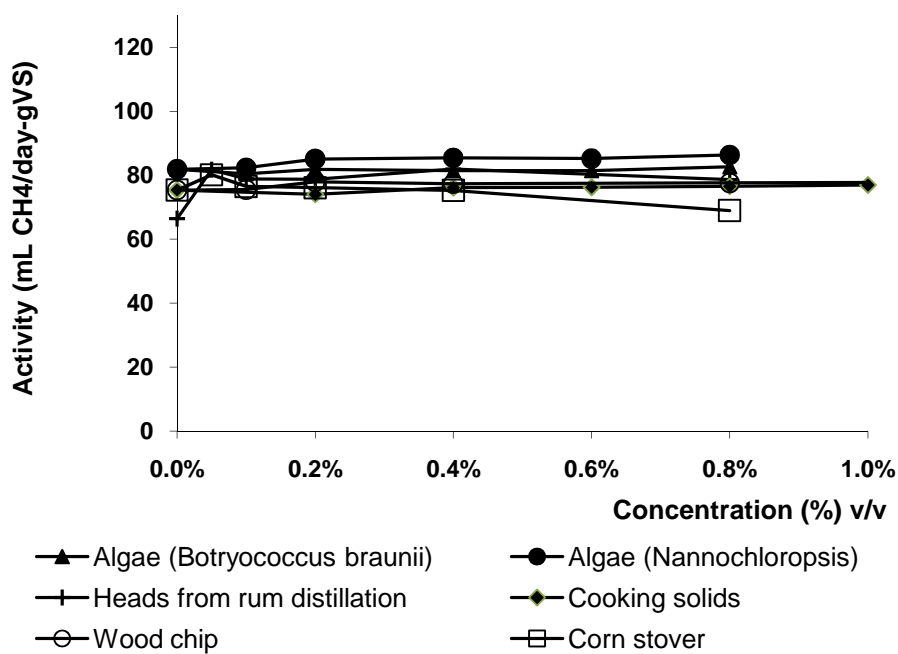


Figure 1.11: (b) Neutral outcomes

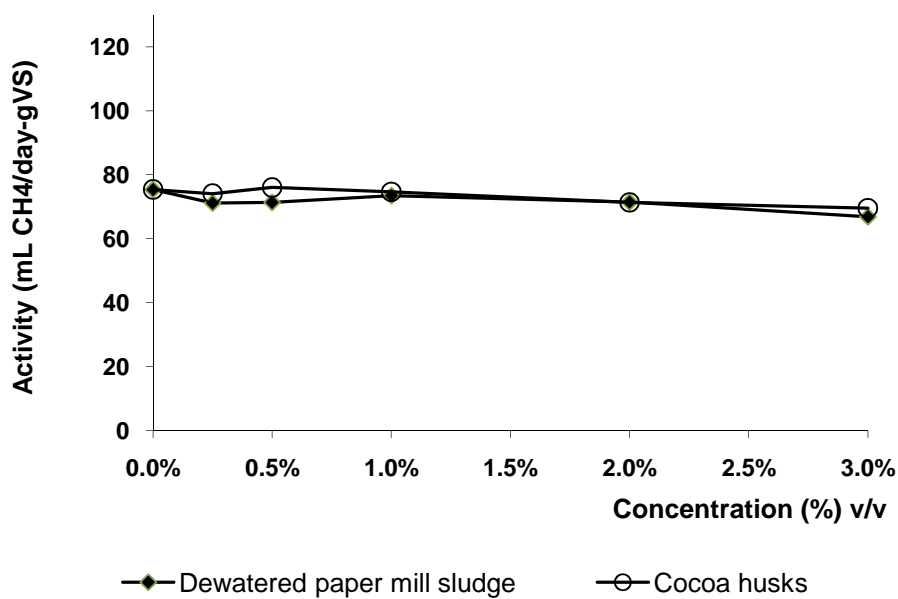


Figure 1.11: (c) Neutral outcomes

Some wastes such as flavorings yeast, trube, brewery yeast, pine apple, corn/rye/wheat/barley in liquid, FT reactor condensate demonstrated mixed outcomes, with a synergistic effect observed at low concentrations and an antagonistic effect observed at higher concentrations (see Figure 1.12 (a) and (b)).

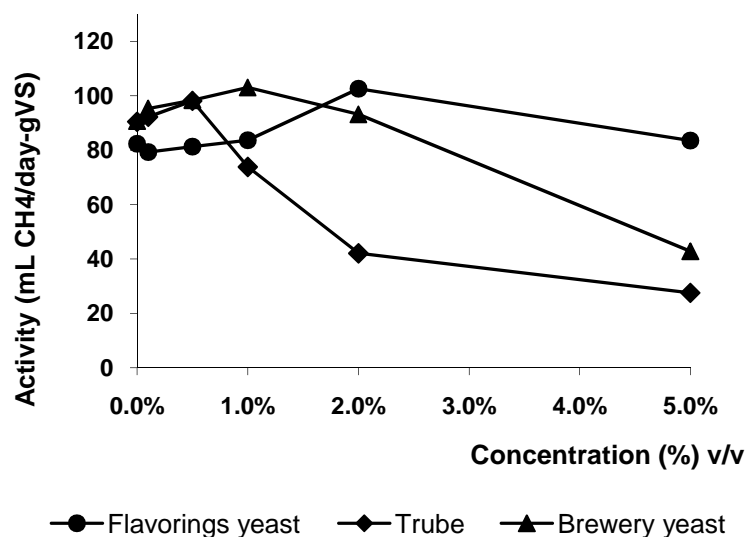


Figure 1.12: (a) Mixed outcomes

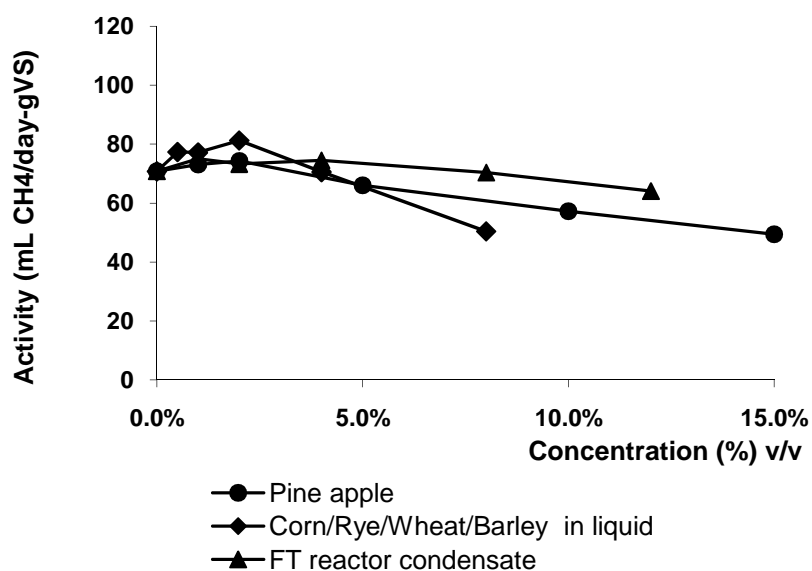


Figure 1.12: (b) Mixed outcomes

1.3.2.4 Sieve analysis

The d_{10} (sieve opening size passing 10% of the material), d_{50} and d_{90} were calculated from the plots of percent passing versus sieve size. The values for d_{10} , d_{50} and d_{90} are presented in Table 1.7 (summary of wastes characteristics). The d_{90} for wastes which were selected for bench scale co-digestion (float, flavorings yeast, thin stillage, acid whey and can crushing wastes) were less than 0.075 mm except float waste. It was 0.52 mm for float waste. The advantages of selecting waste with fine particle sizes were avoidance of grinding of waste as pretreatment, less settling of particles in the available, but unmixed storage tank at SSWRF and easy mixing with primary sludge.

1.3.2.5 Cost-benefit analysis

The cost benefit calculations for 46 wastes are presented in Table A.1 of Appendix A. Only 22 wastes were considered for further screening due to limitation and capability of the existing equipment including pump, mixer at the SSWRF during period of this study. The net benefits for 22 wastes are presented in Figure 1.13. The economic analysis resulted in high positive benefits ($> 50 \text{ \$/m}^3$ of waste) for eight of the 22 co-digestates: (1) heads from rum distillation, (2) syrup, (3) brewery yeast, (4) flavorings yeast, (5) trube, (6) float, (7) corn/rye/wheat/barley in liquid and (8) whole stillage. However, to select co-digestates for further study, other waste characteristics were considered, including the volume of waste produced, the probable reliability of waste availability over time, apparent toxicity, and availability of other sustainable disposal methods (i.e., sale as animal feed or food additive). Based upon all factors, the

five most promising wastes for further bench- and pilot-scale testing were as follows: (1) float, (2) flavorings yeast, (3) thin stillage, (4) acid whey and (5) soft drinking can crushing waste. Even though the net benefits of trube and brewery yeast were positive, these wastes were not included in pilot testing due to low production volume and existing worth as a food product, respectively. Heads from rum distillation, corn/rye/wheat/barley in liquid, molassess wash and sorghum were not included in pilot testing due low production volume (< 20 gpd). Among the four corn ethanol wastes (wet distillers grain, whole stillage, thin stillage and syrup), thin stillage was selected for further study since alternative disposal options were available for whole stillage by separating wet distillers grain (animal feed) and a significant amount of energy is required to produce syrup (syrup is produced from thin stillage by evaporating the water). Oil and hydrolic fluids was not selected because of their antagonistic outcomes. The net benefit of FT reactor condensate was negative because of the high shipping cost resulted from the long distance (1500 km) between the source of waste and the wastewater treatment facility.

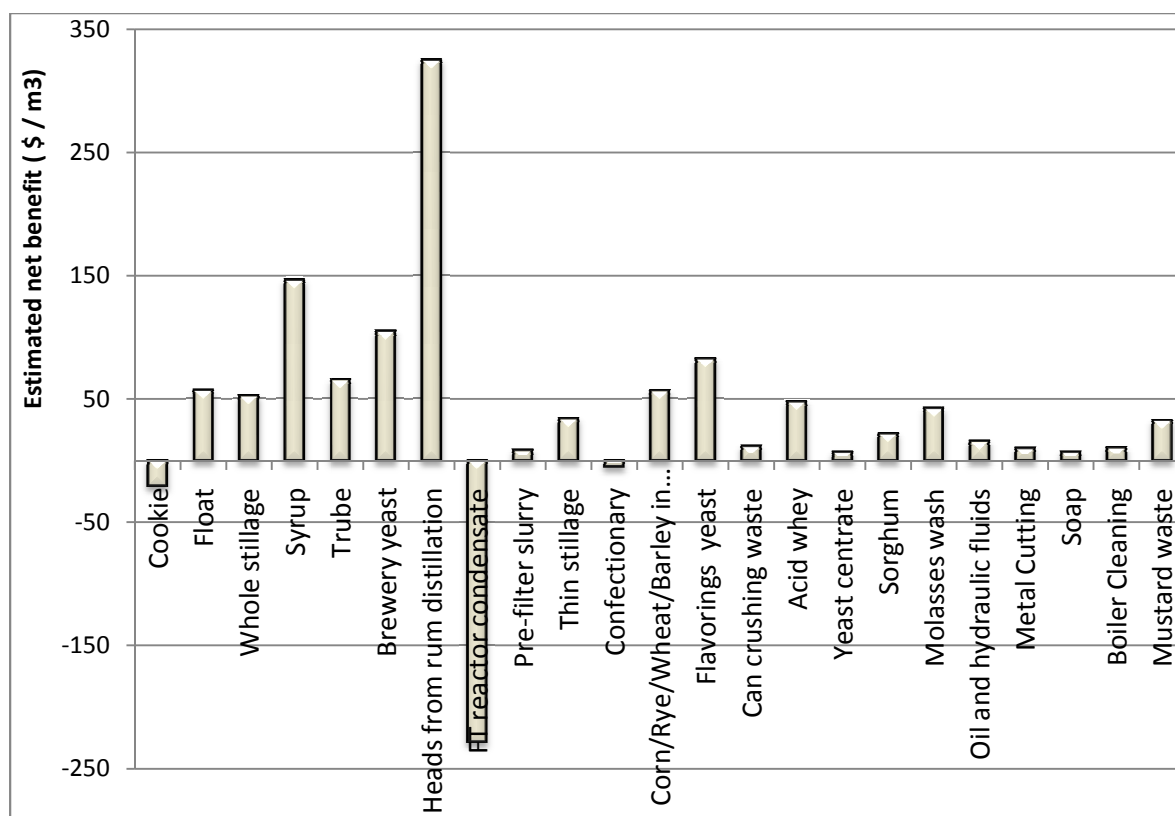


Figure 1.13: Co-digestate cost-benefit analysis results

1.3.3 Performance of bench-scale anaerobic digesters

The performance of bench-scale co-digesters is described below.

1.3.3.1 CH₄ production and biogas composition

The average CH₄ production rates of Control, Co-Digester 1 and Co-Digester 2 systems are presented in Figure 1.14. The CH₄ production rates of all six digesters between Days 45 and 55 were approximately equal. During the co-digestion period (Days 55 to 100), CH₄ production rates of Co-Digester 1 and 2 systems increased by 105% and 66% in comparison to the Control systems, respectively. When extra organic carbon was added to co-digesters, the CH₄ production rate was expected to increase. But the extra

CH_4 production from the additional co-digestate carbon was theoretically anticipated to be only 57% and 23% greater from Co-Digester systems 1 and 2, respectively (see Table 1.8). The theoretical CH_4 production rate was the anticipated CH_4 production from the co-digestates, which was calculated from the corresponding BMP value of the waste. There was a significant synergistic effect when the wastes were co-digested.

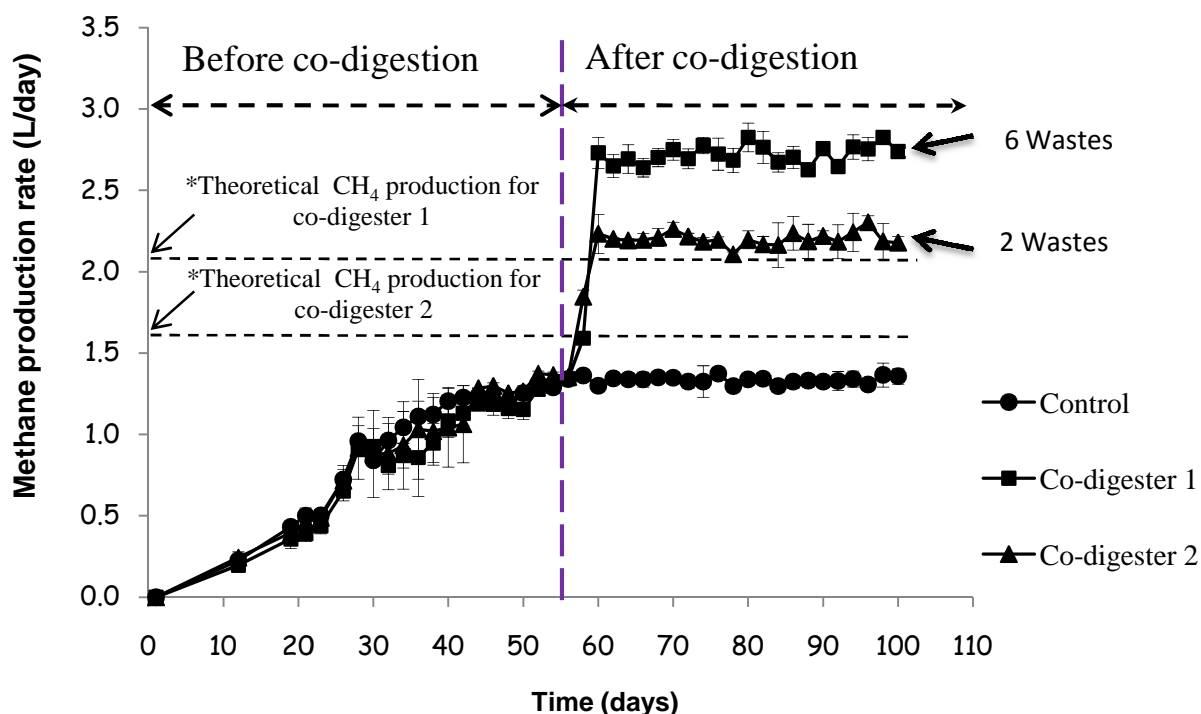


Figure 1.14: CH_4 production rate of digesters

Theoretical CH_4 production = CH_4 production from control + theoretical CH_4 production of co-digestates which was calculated using BMP values of co-digestates

Table 1.8: Methane production due to synergism of co-digestion

	Control	Co-Digester 1	Co-Digester 2
Actual CH ₄ production (L/day)	1.33±0.02	2.73±0.06	2.21±0.04
Theoretical CH ₄ from co-digestates (L/day)	0	0.76±0.02	0.31±0.04
% extra CH ₄ from co-digestates in comparison to Control	-	57±2 %	23±3 %
Theatrical total CH ₄ (L/day)	1.33±0.02	2.09±0.06	1.64±0.06
excess CH ₄ due to the synergism (L/day)	0	0.64±0.08	0.57±0.07
% Excess CH ₄ due to the synergism in comparison to Control	-	48±6 %	42±5 %

1.3.3.2 Biogas methane composition

The biogas CH₄ content was $62 \pm 1\%$ under all three digester conditions.

1.3.3.3 TS and VS destruction

The VS content of the digested sludge from the Control, Co-Digester 1 and Co-Digester 2 systems are presented in Figure 1.15. Average effluent VS concentrations for all the three systems between days 45 and 55 were to around 1%. After steady state with co-digestion, TS removal efficiency of the Control, Co-Digester 1 and Co-Digester 2 systems were 46±2%, 73±3% and 61±3%, respectively. VS removal efficiency of the Control, Co-Digester 1 and Co-Digester 2 systems were 58±2%, 88±3% and 78±2%, respectively. The TS and VS removal efficiencies of Co-Digesters 1 and 2 increased by 49±6 and 33±5, respectively, in comparison to the control systems.

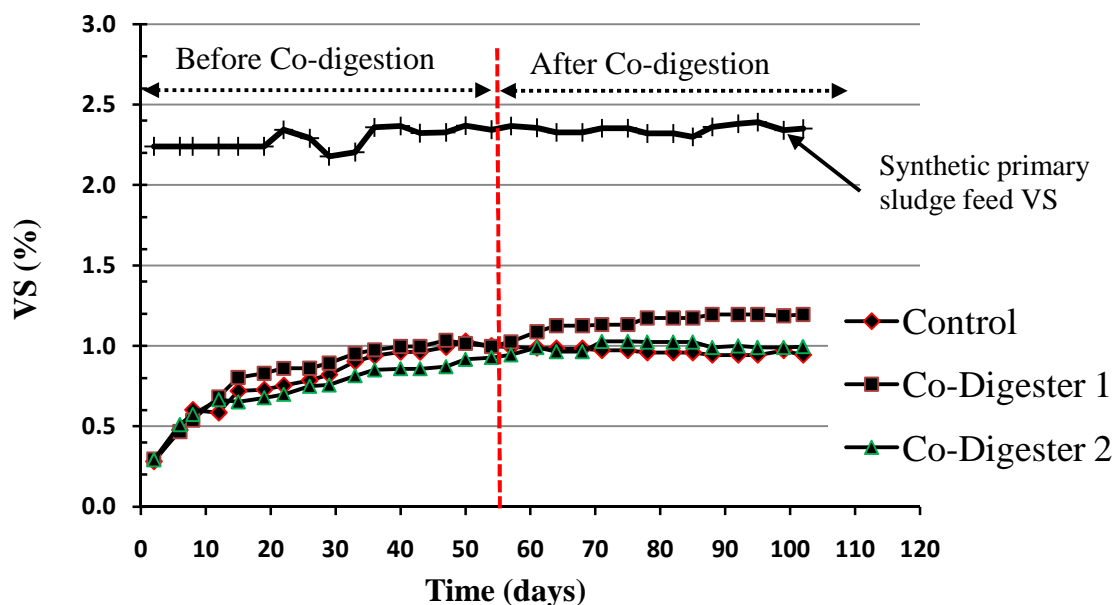


Figure 1.15: VS of digested sludge versus operation time

1.3.3.4 Other effluent values

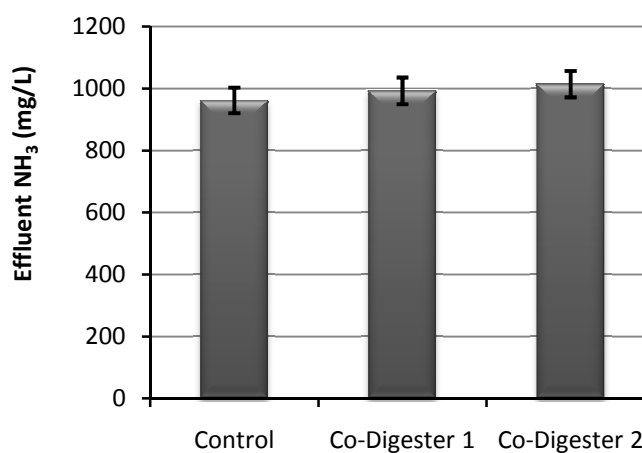
The values for pH, total VFA, alkalinity, soluble COD and soluble TOC for all three conditions are listed in Table 1.9. The parameters, pH, total VFA, alkalinity and SCOD in Table 1.9 were not statistically different among the three digester systems. TSS and VSS were statistically different between Control and Co-Digester 1 systems, whereas not statistically different between Control and Co-Digester 2 systems. The Soluble TOC was statistically different among the three digester systems.

Table 1.9: Effluent values for all three conditions

Parameters	Control	Co-Digester 1	Co-Digester 2
pH	7.2-7.3	7.2-7.3	7.2-7.3
Total VFA (eq/L)	0.29 ± 0.14	0.23 ± 0.16	0.30 ± 0.10
Alkalinity (mg/L as CaCO ₃)	6000 ± 50	6010 ± 40	5990 ± 70
SCOD(mg/L)	970 ± 90	1160 ± 110	980 ± 110
Soluble TOC (mg/L)	940 ± 20	1142 ± 20	1030 ± 30
TSS (g/L)	9.83 ± 0.27	12.9 ± 0.8	9.95 ± 0.70
VSS (g/L)	8.36 ± 0.44	10.8 ± 0.4	8.38 ± 0.74

1.3.3.5 NH₃-N and TKN

Effluent NH₃-N and TKN concentrations under all three conditions were between 910-1050 mg/L and 1510-1860 mg/L respectively (see Figure 1.16 (a) and (b)). The Average TKN/NH₃-N ratio was 1.7. Average NH₃-N and TKN concentrations, in order from highest to lowest were as follows: Co-Digester 2 > Co-Digester 1 > Control. However, NH₃-N and TKN concentrations in the Control and Co-Digester 1 systems were not significantly different, whereas those of the Control and Co-Digester 2 systems were different at a 99% level of significance.

**Figure 1.16: (a) Effluent NH₃-N concentration under three conditions**

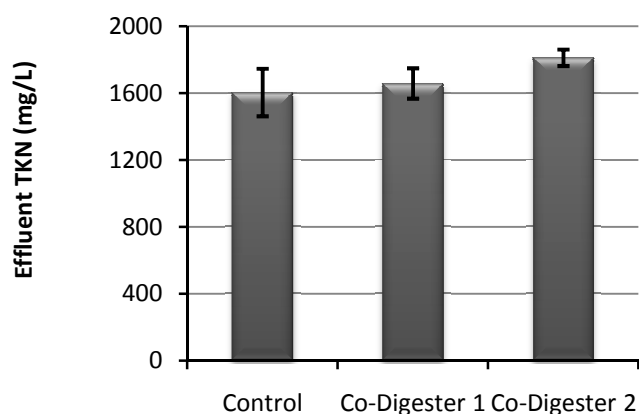


Figure 1.6: (b) Effluent TKN concentration under three conditions

1.3.3.6 Estimated benefit of full scale co-digestion based on bench-scale digester

Bench-scale digester results were used to estimate the energy production and CO₂ avoidance for full-scale co-digestion (see Table 1.10). The full-scale Co-Digester 1 scenario involves a feed volume including 1890 m³/d primary sludge, 38 m³/d float, 12 m³/d flavorings yeast, 61 m³/d thin stillage, 45 m³/d acid whey, and 36 m³/d can crushing waste. The Co-Digester 2 scenario involves a feed volume including 1890 m³/d primary sludge and 12 m³/d flavorings yeast. Co-digester 1 and 2 scenarios were estimated to result in a decrease in net CO₂ emissions assuming that biogas replaces coal as fuel (see Table 1.10). The additional electricity generated from Co-Digester 1 and 2 scenarios was estimated to be enough to power more than 2500 and 340 houses, respectively. However, actual full-scale energy production and CO₂ emissions may vary due to other factors.

Table 1.10: Estimated energy production and CO₂ avoidance

	Control	Co-Digester 1	Co-Digester 2
Primary sludge flow (m ³ /day)	1890	1890	1890
Co-digestate flow (m ³ /day)	0	192	12
Total CH ₄ (ML/day)	15.1	34.1	17.7
CH ₄ energy (1000MJ/day) ^a	530	1190	620
Estimated CO ₂ emissions avoidance ^b (tonnes/year)	17000	38200	19900
Average U.S. homes provided electricity ^c (houses)	2000	4500	2340

^a Assuming CH₄ heat content of 0.035 MJ/L CH₄ at 35°C (930 BTU/ft³)

^b Assuming switching from bituminous coal and coal emissions factor of 0.088 kg CO₂/MJ (Hong and Slatick, 1994)

^c Assuming average U.S. household electricity usage of 90 MJ/d (25kWh/d) and biogas-to-electricity conversion efficiency of 34% (10000 Btu/kWh) (Speece, 1996)

1.3.4 Specific methanogenic activity (SMA) of biomass

The SMA values of biomass from each of the six bench-scale digesters were calculated from triplicate assays. The SMAs for the duplicate digesters in each system were not statistically different. Therefore, all six SMA measurements for each system were averaged. The SMAs against each substrate (acetate, propionate and hydrogen) are described below.

1.3.4.1 SMA against acetate and propionate

The SMAs against acetate as a substrate are presented in Figure 1.17. Error bars represent the standard deviation of the six SMAs for each system. The highest SMA values were obtained for the biomass taken from the Co-Digester 1 systems, whereas Co-Digester 2 biomass also demonstrated SMA values higher than the Control systems. The increases in average SMA value of the biomass due to co-digestion were 19±9 % and 18±9 % for Co-Digester 1 and 2 systems, respectively, compared to the Control systems.

The SMAs were statistically different at the 99% significance level between Control and Co-Digester 1($F(1, 10) = 31$ and $\alpha < 0.001$) as well as Control and Co-Digester 2($F(1, 10) = 28.9$ and $\alpha < 0.001$).

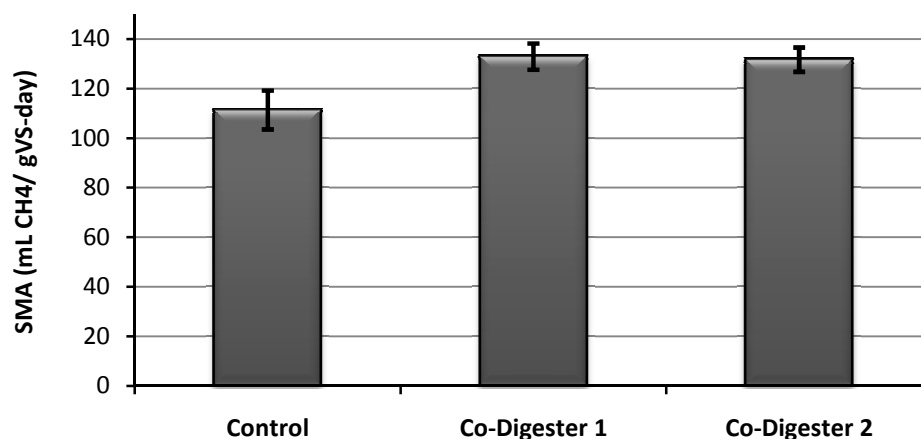


Figure 1.17: SMA results against acetate of the different conditions

The SMAs against propionate as a substrate are presented in Figure 1.18. Error bars represent the standard deviation of the six SMAs for each condition. Higher SMAs were obtained for the biomass taken from Co-Digester 1 and 2 systems. The increases in SMAs of the biomass due to co-digestion were 27 ± 12 % and 32 ± 16 % for the Co-Digester 1 and 2 systems, respectively, compared to the control. The average SMA values were statistically different at the 99% significance level between Control and Co-Digester 1($F(1, 10) = 31.8$ and $\alpha < 0.001$) as well as Control and Co-Digester 2($F(1, 10) = 26.6$ and $\alpha < 0.001$).

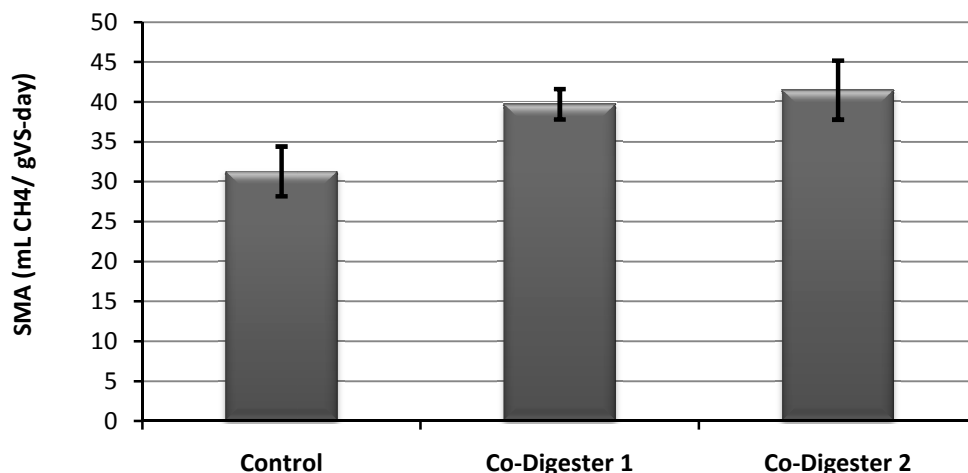


Figure 1.18: SMA results against propionate of the different conditions

1.3.4.2 SMA against H₂

The SMAs against H₂ as a substrate are presented in Figure 1.19. Error bars represent standard deviation of the six SMAs for each condition. The higher SMAs were obtained for the biomass taken from the Co-Digester 1 and 2 systems. The increases in SMA values of the biomass due to co-digestion were 36 ± 19 % and 15 ± 25 % for Co-Digester 1 and 2 systems, respectively, compared to the Control. The SMAs were statistically different at the 99% significance level between Control and Co-Digester 1 systems ($F(1, 10) = 22.5$ and $\alpha = 0.001$), whereas the SMAs were not statistically different at the 95% significance level between the Control and Co-Digester 2 systems ($F(1, 10) = 2.3$ and $\alpha = 0.16$).

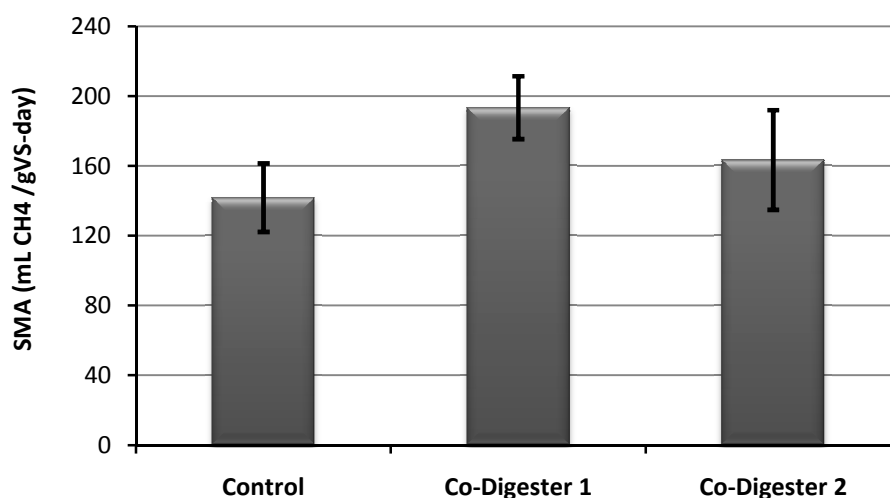


Figure 1.19: SMA results against H₂ of the biomass from the different digesters

In three cases, the SMA values against acetate, propionate and H₂, the SMAs of biomass in the co-digesters increased compared to that of the controls. The reasons for increased SMAs may be either an increase in the total number of microbes present in co-digesters (but the same general microbial community structure), the establishment of a new microbial community structure in co-digesters, or both. The microbial community structures in different digesters can be compared using molecular techniques like denaturing gradient gel electrophoresis (DGGE), quantitative polymerase chain reaction (qPCR) or other methods. The relationship among DGGE banding pattern of methyl coenzyme M reductase (*mcrA*) genes and increased SMAs is described in the Chapter 2. The increase in SMA may be a cause for synergistic outcomes in the co-digesters.

1.3.5 Synergistic, antagonistic and neutral outcomes for different wastes

The BMP results for single and mixtures of two wastes are presented in Table

1.11. High BMP values were observed for these wastes except for the BMP of metal cutting waste and metal cutting waste with synthetic primary sludge.

Table 1.11: BMP results for single and mixed wastes

Samples	Average CH ₄ mL/g COD	Std-deviation CH ₄ mL/g COD
Flavorings	318	16
Thin stillage	364	7
Acid whey	347	5
Can crushing	338	8
Metal cutting	117	5
Float	390	8
synthetic primary sludge	367	13
synthetic primary sludge + Flavorings	386	9
synthetic primary sludge + Thin stillage	394	6
synthetic primary sludge + Acid whey	387	6
synthetic primary sludge + Can crushing	391	7
synthetic primary sludge + Metal cutting	218	10
synthetic primary sludge + Float	383	6

For actual BMP values determined for mixed wastes, a 50/50 mass blend based on COD was tested. Theoretical BMP values of the mixed wastes (i.e., the sum of 50% of the BMP values of each waste in the mix) were also calculated. Both the actual BMP and theoretical BMP values for each waste mix are presented in Figure 1.20. The actual BMP value of mixed waste was $13 \pm 7\%$ greater than the theoretical value for flavorings waste, $11 \pm 5\%$ for can crushing waste, and $8 \pm 4\%$ greater for acid whey and thin stillage. On the other hand, there were a decrease between actual and theoretical BMP values for mixes of synthetic primary sludge and metal cutting waste, whereas there was no difference for

the float waste. Therefore, flavorings yeast, thing stillage, acid whey and can crushing wastes demonstrated synergistic outcomes, metal cutting waste demonstrated an antagonistic outcome and float waste demonstrated a neutral outcome. Similar results, synergistic, antagonistic or neutral outcomes for each waste mixed with acetate as main unlimited substrate were obtained from previous anaerobic toxicity assays, except for the acid whey. This BMP test revealed that acid whey was a synergistic waste, whereas it was neutral in the anaerobic toxicity assay. A reason for this may be that in BMP test, acid whey showed synergism with the synthetic primary sludge, whereas it showed neutral outcome because acetate was used as co-substrate in the anaerobic toxicity assay.

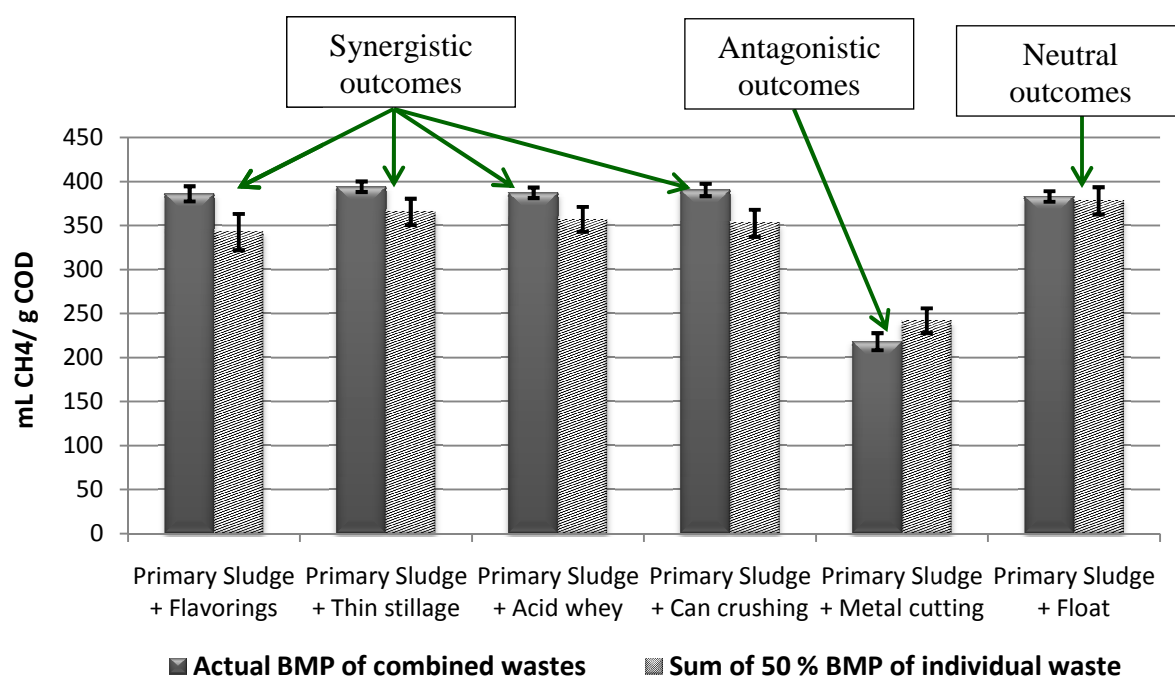


Figure 1.20: Different co-digestion outcomes

1.3.6 Full-scale co-digestion testing at SSWWRF

The characteristic of acid whey used as a co-digestate in the full-scale co-digestion is presented in Table 1.12. Typical acid whey wastes generated in other cheese factories were reported to contain up to 70 g/L COD, some carbohydrates (4-5%) and mainly lactose (Mawson, 1994; Gelegenis et al., 2007). A similar value (60 g/L) was observed for COD of the acid whey in this study. Moreover, no alkalinity was observed in this study. Primary sludge feeding flow rate and TS and VS loading rates are presented in Table 1.13. All performance parameters of digesters were reported over 171 days of operation, including a control period of 60 days, a subsequent co-digestion period of 61 days and a post co-digestion period of 50 days. The post co-digestion period was limited to 50 days because CH₄ production rate reached the value equal to the average CH₄ production rate in the control period, and because another co-digestate (can crushing waste) was fed just after the post co-digestion period. Can crushing volumes were very low (2000 gallons /week) and can crushing waste testing was stopped. No data on can crushing waste digestion are reported herein.

Table 1.12: Acid whey characteristics in full-scale digestion testing

Parameters	Value	Number of data (n) used
COD (g/L)	59.3±7.4	21
pH	3.7± 0.4	16
TS (%)	6.6± 1.5	22
VS/TS (%)	86.5± 1.6	22
NH ₃ -N (mg/L)	120± 20	18
TKN (mg/L)	650± 50	18

Table 1.13: Primary sludge flow rate and TS and VS loading rates

		SSPS¹ Flow to digesters MGD	JIPS² flow to digesters Total	TS input	VS input	Total VS feed /week	Total TS feed /week
Date	Days	MG/week	MG/week	(%)	(%)	tones VS /week	tones TS /week
4/27/2010	4	1.22	1.51	2.42	1.82	273.59	363.09
5/4/2010	11	1.31	1.12	2.49	1.92	272.02	352.26
5/11/2010	18	1.16	1.52	2.38	1.82	265.53	346.73
5/18/2010	25	1.38	1.90	2.73	1.94	341.45	480.52
5/25/2010	32	1.34	0.85	2.84	2.13	284.87	381.18
6/1/2010	39	1.19	1.23	3.16	2.38	325.14	431.35
6/8/2010	46	1.24	1.04	2.96	2.21	295.37	394.27
6/15/2010	53	1.23	1.07	3.15	2.37	317.31	422.11
6/22/2010	60	1.21	1.93	2.77	1.99	328.92	457.09
6/29/2010	67	1.10	1.34	2.58	1.74	234.00	346.02
7/6/2010	74	1.29	1.25	2.26	1.65	238.81	327.56
7/13/2010	81	1.43	0.29	2.79	2.06	245.58	332.60
7/20/2010	88	1.30	1.07	2.64	1.71	238.00	367.73
7/27/2010	95	1.26	1.50	3.17	2.04	310.66	482.18
8/3/2010	102	1.47	2.19	3.02	1.95	379.65	587.36
8/10/2010	109	1.42	2.81	3.56	2.33	499.54	761.15
8/17/2010	116	1.85	0.62	3.38	2.36	387.73	554.56
8/24/2010	123	1.64	0.10	2.89	2.18	280.73	370.84
8/31/2010	130	1.58	0.13	2.61	2.04	253.98	324.22
9/7/2010	137	1.61	0.18	2.99	2.31	298.12	385.68
9/14/2010	144	1.60	0.13	2.79	2.19	276.01	352.01
9/21/2010	151	1.53	1.35	2.55	1.91	318.82	426.07
9/28/2010	158	1.79	0.74	2.59	1.98	323.81	425.27
10/5/2010	165	1.82	1.07	2.60	2.01	358.07	463.42
10/12/2010	172	1.72	0.00	2.40	1.85	241.71	313.94

¹SSPS: SSWWRF Primary sludge²JIPS: Jones Island wastewater reclamation facility Primary Sludge

1.3.6.1 Methane production rate

Daily biogas production and co-digestate flow rate are presented in Table A.2 of Appendix A. CH₄ production rate and acid whey feed rate are presented in Figure 1.21. The average CH₄ production rate during the control period was 8700 m³/day which is presented as a horizontal line on Figure 1.21. When the co-digestate feeding was started, an increase in biogas production was expected. However, there was not a significant increase in CH₄ production rate until Day 100. It may be because of a decreased VS content of the primary sludge between Days 55 and 75 (see Figure 1.23). Unfortunately, there was not precise control of TS and VS concentration of the primary sludge feed. However, average VS content of the primary sludge remained in the range of 1.6 -2.4 %. Average CH₄ production per kg VS of primary sludge added during the control period was 0.21 m³/ kg VS_{input}. This value was used to calculate theoretical CH₄ production from primary sludge during the co-digestion and the post co-digestion periods. Excess CH₄ gas volumes of 91,000 m³ and 124,000 m³ were estimated by calculating the difference between theoretical and actual CH₄ production over co-digestion and post co-digestion respectively (see Table A.3 of Appendix A). However a maximum of only 21,000 m³ could have been produced from COD of the acid whey co-digestate added based on a stoichiometric maximum of 400 m³ CH₄/kg of COD (35°C, 1 atm). Therefore co-digestion of the synergistic co-digestate, acid whey, increased CH₄ production by an extra 194,000 m³ over the co-digestion and the post co-digestion periods. In overall the full scale co-digestion of acid whey in addition to primary sludge increased methane production by 21 % (19% from synergism and 2% predicted from COD of acid whey) over co-digestion and post co-digestion periods.

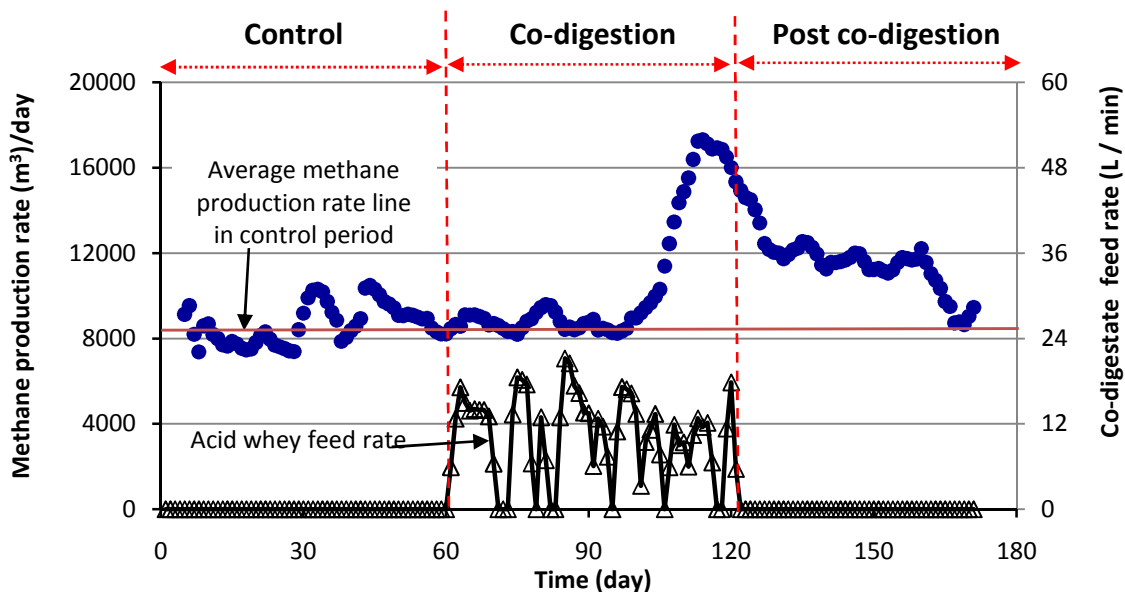


Figure 1.21: CH₄ production rate and co-digestate feed rate
(CH₄ production rate: circle, 7 days running average)

1.3.6.2 Percent of methane in the biogas

Average percent of CH₄ in the biogas from the five digesters is presented in Figure 1.22. The average percent of CH₄ values for the control, co-digestion and post co-digestion periods were 55 ± 3 , 58 ± 2 and 59 ± 1 , respectively. Percent of CH₄ in the co-digestion and post co-digestion periods were statistically different from percent of CH₄ in the control period at the 5% significance level ($\alpha < 0.05$). The percent of CO₂ in the biogas was approximately 28-29 % for all periods. Co-digestion of synergistic waste increased the present of CH₄ in the biogas by 5% during the co-digestion period and by 7% during the post co-digestion period as well.

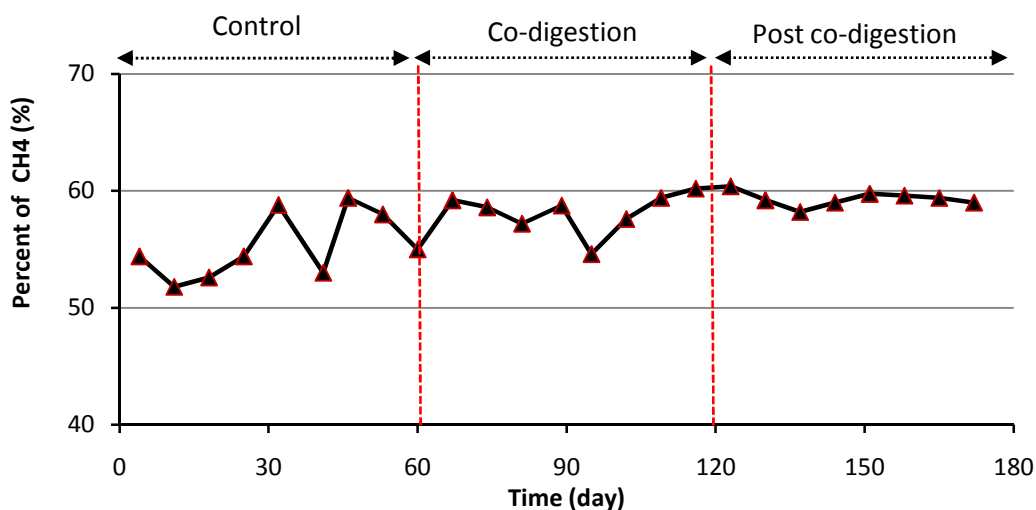


Figure 1.22: Average percent of CH₄ in the digesters' biogas

1.3.6.3 TS and VS removal

The influent and effluent VS content for the digesters are presented in Figure 1.23. TS removal efficiency was 30% in the control, 33% in the co-digestion and 33% in the post co-digestion periods (see Table A.4 of Appendix A). VS removal efficiencies were 32% in the control, 34% in the co-digestion and 39% in the post co-digestion periods (see Table A.5 of Appendix A). The TS and VS reduction was 20 and 28% greater, respectively during and after co-digestion.

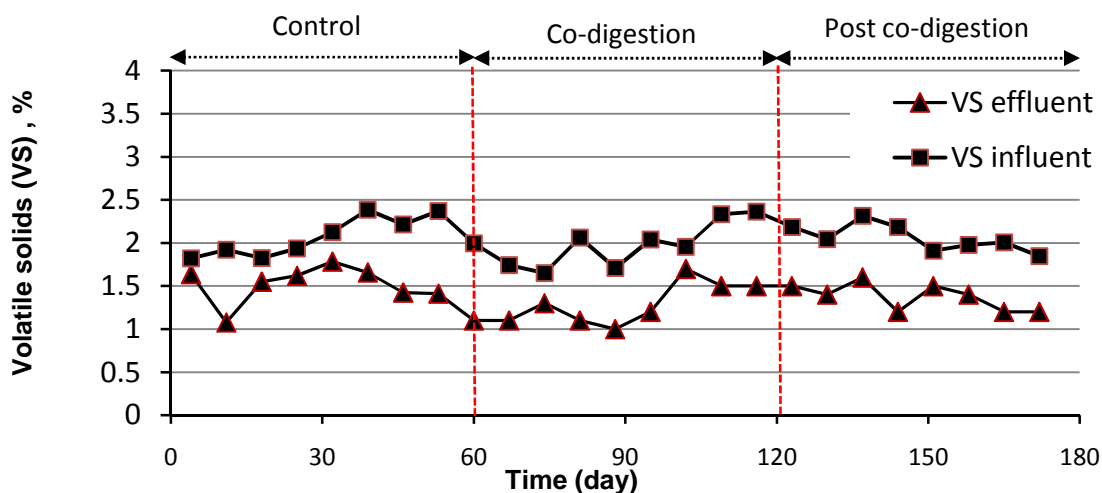


Figure 1.23: Average percent of CH₄ in the digesters' biogas

1.3.6.4 pH, temperature alkalinity and VFA production

Average pH, temperature and alkalinity of each digester are presented in Table 1.14. Values for temperature, pH and alkalinity were within the typical range of anaerobic digestion of municipal sludge. A stable digester has a minimum safe pH value of 6.8 (Speece, 2008) and a total alkalinity of 2000 to 5000 mg/L (WEF, 1996). Therefore, all digesters were operated in a stable condition.

Table 1.14: Temperature and alkalinity of digesters

Digesters	pH	Temperature (°C)	Alkalinity (mg/L as CaCO ₃)
D6	6.9 ± 0.3	35 ± 5	1500 ± 200
D8	6.9 ± 0.4	35 ± 7	1500 ± 200
D10	7.1 ± 0.4	37 ± 2	1800 ± 500
D11	7.0 ± 0.4	36 ± 2	1800 ± 200
D12	7.0 ± 0.4	37 ± 1	1800 ± 200

A plot of total VFA concentration in each digester versus time is presented in Figure 1.24. Unfortunately, some VFA measurements (not shown in Figure 1.24) during the control period were more than 500 mg/L. They were ostensibly sampling or analytical errors and not considered in the analysis. The total VFA concentrations of all the digesters were less the 300 mg/L during the co-digestion and post co-digestion periods. Since a typical value of VFA of a well-established anaerobic digester is less than 500 mg/L, all the digesters were under the typical limit during co-digestion and post co-digestion periods.

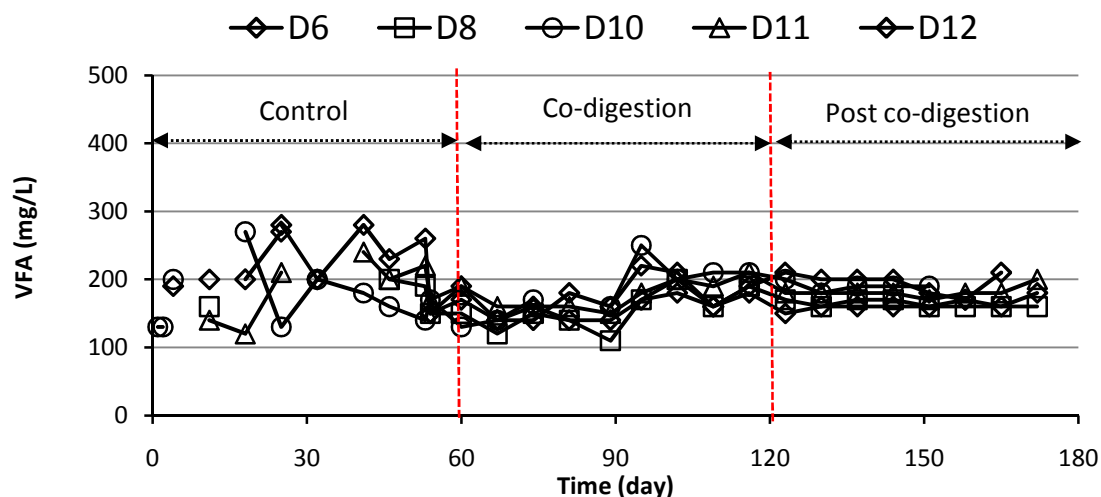


Figure 1.24: Volatile fatty acids (VFA) of each digester

1.3.6.5 $\text{NH}_3\text{-N}$ and TKN of digested sludge

The $\text{NH}_3\text{-N}$ and TKN concentrations of digested sludge during the co-digestion period were 250 ± 40 and 1060 ± 270 mg/L, respectively. The ratio TKN/ NH_3 was found to be 4.2. Unfortunately, $\text{NH}_3\text{-N}$ and TKN concentrations of digested sludge during the control and post co-digestion periods were not measured.

1.3.6.6 Mass balance

The VS mass balance of digesters is presented in Table 1.15. VS input into the digesters, VS output from the digesters, accumulation in the digesters and ostensibly destroyed by anaerobic degradation were accounted for in the mass balance. CH_4 yields from VS destroyed were estimated to be 650, 704 and 676 L CH_4 / kg $\text{VS}_{\text{destroyed}}$ in the control, co-digestion and post co-digestion periods, respectively. The CH_4 yield per VS destroyed during co-digestion increased by 8% in comparison to the control. Specific CH_4 yield calculated in this study was within the typical range reported by Metcalf and

Eddy (2003) and WEF (1998). Metcalf and Eddy (2003) stated that typical CH_4 yield varies from 420 to 840 L CH_4 / kg VS destroyed for the anaerobic digestion process.

WEF (1998) reported that CH_4 production for various substrates as follows (m^3 CH_4 per kg volatile solids destroyed): fats, 0.74 to 1.15; scum, 0.63 to 0.75; grease, 0.75; fibers 0.36 to 0.40; protein 0.51; and typical primary sludge and activated sludge, 0.48 to 0.7.

Table 1.15: VS mass balance of digesters

	Control	Co-digestion	Post co-digestion
Period considered (days)	60	61	50
Total VS added (tonne VS)	2,560	2,810 ¹	2,130
Total VS wasted (tonne VS)	1,860	1,820	1,430
VS accumulation (tonne VS)	-120	50	-140
VS destroyed (Tonne VS)	820	940	840
Total CH_4 produced (KCF)	18,800	23,400	20,000
Total CH_4 produced (KL)	533,000	663,000	567,000
L CH_4 /kg VS destroyed	650	704	676

¹ value included 50 tonne of VS of acid whey added to the digesters

1.4 Conclusions

This study was performed to help develop a method/protocol to select the most promising co-digestates for full-scale co-digestion. This method included four steps: (1) preliminary screening (market survey), (2) waste characterization (BMP, ATA, sieve analysis, other tests including analyses of a suite of metals), (3) simple economic analysis, and (4) bench-scale digester testing. Co-digestion outcomes can be categorized as synergistic, neutral, antagonistic based on the biogas production rate for digestion of more than one co-digestate being greater than, the same as, or less than that observed as a sum of CH_4 production rate when each waste is digested alone.

The co-digestion of five wastes (float, spent yeast, thin stillage, acid whey and soft drink can crushing waste) in addition to primary sludge is feasible at full-scale. Co-digestion of these wastes increased biogas production significantly more than the value predicted based upon their BMP values alone. Co-digestion of the most promising wastes with primary sludge in full scale was estimated to generate enough electricity (renewable energy) to power >2500 houses more than primary sludge digestion alone. Co-digestion in full-scale was estimated to decrease CO₂ emissions. The co-digestion of most promising waste increased specific methanogenic activities (SMAs) against acetate, propionate and hydrogen as a substrate.

The full scale co-digestion of acid whey in addition to primary sludge increased CH₄ production by 21 % (19% from synergism and 2% predicted from COD of acid whey), percent of CH₄ by 5%, CH₄ yield per VS destroyed by 8% (from 650 to 704 L CH₄ / kg VS_{destroyed}), total solids and volatile solids removal efficiency by 20%. In conclusion, co-digestion is one method to increase renewable energy production and decrease GHG emission via anaerobic digestion.

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Chapter 2

Anaerobic co-digestion with synergistic waste increases microbial activity and changes the microbial community

Anaerobic co-digestion is a process in which a mixture of at least two different high- strength wastes is digested, producing more biogas as a source of renewable energy. Appropriate waste selection and optimum blending ratios can help maximize biogas production in co-digestion. The right balance of macro- and micro-nutrients, pH, inhibitory/toxic compounds, biodegradable organic matter and dry matter in a waste mixture is important for co-digestion performance (Hartmann et al., 2003). Co-digestion with any combination of wastes can result in synergistic, antagonistic and neutral outcomes depending on waste composition (Zitomer et al., 2008). The synergistic, antagonistic and neutral outcomes of co-digestion can be defined based upon methane (CH_4) production that is greater than, less than or the same as that observed when each material is digested alone. Reasons for synergistic outcomes include improved nutrient balance, bio-availability of trace metals by complex agents in waste and others. The exact mechanism and fundamental reason for a synergistic outcome has not been clear defined. Most recent co-digestion research involves relationships between process performance and operating parameters and optimization of blending ratios. However, it is also important to study the influence of co-digestion on microbial communities. There is little research reported to understand the link between digester performance and microbial community structure in an anaerobic digester, and, to the author's knowledge, none involving co-digestion and microbial community.

The degradation of organic compounds to carbon dioxide (CO₂) and CH₄ occurs in four discrete steps (Speece 1996). Methanogenesis, the final step, produces CH₄ and CO₂ from either acetate or hydrogen/formate and CO₂ (White 2000). Therefore, investigating the methanogenic community is a potentially valuable tool to determine co-digestion influence on the microbial community. Methyl coenzyme M reductase (*mcrA*) is the enzyme that catalyzes the final reaction in the methanogenesis pathway (Ermler et al. 1997). Therefore, the *mcrA* functional gene has been used to understand methanogenic community structure in various microbial samples. The community structure and diversity of methanogens should be investigated using molecular fingerprinting techniques to compare biomass samples from control (without co-digestion) and co-digestion systems. Several molecular techniques can be used including denaturing and temperature gradient gel electrophoresis (DGGE and TGGE), single strand conformation polymorphism (SSCP), terminal-restriction fragment length polymorphism (tRFLP), 16S rRNA gene cloning and pyrosequencing. Among these techniques, DGGE is one of the most well established molecular tools for biodiversity assessment in microbial ecology (Head et al., 1998; Muyzer and Smalla, 1998; Boon et al., 2002; Stamper et al., 2003; Arooj et al., 2007). Further, comparison and calculation of biodiversity indices (e.g. principle component analysis, Simpson's and Shannon-Weaver indices, cluster analysis, etc.) can be used to interpret data from DGGE images (Marzorati et al., 2008).

Recently, the blending of anaerobic co-digestates, synergism and economics has been reported (Navaneethan et al., 2011). In this study, the performance of bench-scale

digesters for 3 systems (Control, Co-Digester 1 and Co-Digester 2) was monitored for six months. Co-Digester 1 and 2 systems were fed with six and two co-digestates, respectively, whereas Control systems were fed with synthetic primary sludge alone. Objectives of this study were to identify co-digestion effect on the microbial activities and microbial community structure.

2.1.1 Research hypothesis

In this study, three main hypotheses were defined as follows:

1. Co-digestion of synergetic co-digestates in addition to primary sludge increases biogas production significantly more than that predicted based upon BMP values alone
2. Co-digestion can increase specific methanogenic activities against acetate, propionate and H₂ as substrates
3. Co-digestion changes the microbial community structure in comparison to control digesters receiving synthetic primary sludge

2.2 Methodology

2.2.1 Specific methanogenic activity

The digester performance or "activity" of microbial cultures was determined using SMA tests of biomass samples against acetate and propionate (Angelidaki et al., 2007) as well as H₂ (Coates et al. 2005; Coates et al. 1996) according to published methods . However, the few modifications made to these methods are described below. Assays were conducted in triplicate at 35°C, 150 rpm using an incubator shaker (model C25KC, New Brunswick Scientific, Edison, NJ). All assays were performed under anaerobic

conditions in 160-ml serum bottles. The VS concentration of the biomass was measured at the beginning of activity tests.

2.2.1.1 SMA against acetate and propionate

Fifteen mL (140-180 mg VS) and 25 mL (240-300 mgVS) of biomass were used in acetate and propionate activity tests, respectively. The final total volume of the assay was kept at 30 mL by adding the appropriate amount of basal media. Bottles were sparged with oxygen-free gas (7:3 v/v N₂:CO₂), closed with solid, black, butyl rubber septa and incubated. Approximately 3 days were allowed for degassing from residual COD in the biomass. CH₄ content in the headspace was measured using gas chromatography (GC). Substrates were injected through the septum using a syringe and needle to achieve a calcium acetate concentration of 12 g/L and a calcium propionate concentration of 3.4 g/L. The biogas volume produced was measured at ambient pressure and 35C every day using a 10- or 100-mL (depending upon gas production) glass syringe with a wetted glass barrel. The syringe content was re-injected into the serum bottle after volume measurement. Headspace CH₄ content was measured by GC at the end of testing.

For acetate and propionate activities, maximum CH₄ production rate (mL CH₄/day) was determined by linear regression of the initial, linear portion of a plot of cumulative CH₄ production versus time. SMA values (mL CH₄/g VS-day) were calculated by dividing maximum CH₄ production rate values by average VS mass.

2.2.1.2 SMA against H₂

A sample of 8 to 12 mg VS of biomass was used in hydrogenotrophic activity tests. The final total volume of the assay was kept at 30 mL by adding the appropriate amount of basal media. Bottles were sparged with oxygen-free gas (7:3 v/v N₂:CO₂), closed with solid, black, butyl rubber septa and incubated. Then, 3 days were allowed for degassing from residual COD in the biomass. Subsequently, 100 mL of an H₂ and CO₂ gas mixture (at a ratio of 1:4, v/v) at ambient pressure and temperature was injected through the septum using a syringe and needle; then the bottles were incubated. Bottle headspace volume was measured by inserting the needle of a glass syringe with wetted barrel at ambient pressure and at 35°C twice a day for 7 days. Syringe content was re-injected into the serum bottle after volume measurements.

For hydrogenotrophic activity, the volume of H₂:CO₂ gas utilized was calculated as from the decrease in the gas volumes in the assay plus the gas volume produced from endogenous control bottles at the given period of time. CH₄ production was estimated as the volume of H₂:CO₂ gas utilized divided by 4 based upon the stoichiometry of CH₄ production from H₂ and CO₂ (1 mol CH₄ produced from every 4 mols H₂ and 1 mol of CO₂). Maximum CH₄ production rate (mL CH₄/day) was determined by linear regression of the initial, linear portion of a plot of cumulative CH₄ production versus time. SMA values (mL CH₄/g VS-day) were calculated by dividing maximum CH₄ production rate values by average VS mass.

2.2.2 Influence of co-digestion on diversity and population of digester microorganisms

Molecular techniques used included denaturing gradient gel electrophoresis (DGGE) and quantitative polymerase chain reaction (qPCR).

2.2.2.1 DNA extraction

DNA was extracted from 0.75 mL of biomass obtained from each bench-scale digester just before co-digestion and 2 and 8 weeks after the beginning of co-digestion. The PowerSoil™ DNA Isolation Sample Kit (MoBio Laboratories, Inc., Carlsbad, CA) was used to extract DNA according to the manufacturer's instructions using the alternative lysis method. This alternative lysis method reduced the horizontal vortexing time of the PowerBead tubes from 10 to 1 minute and employed incubation at 70°C for 10 minutes. This ostensibly reduced shearing of DNA. The presence of extracted DNA was confirmed using agarose gel electrophoresis.

2.2.2.2 Agarose gel electrophoresis

A 1% agarose gel was prepared by mixing agarose with 1X Tris-Acetate-ethylenediaminetetraacetic acid (TAE) buffer. The resulting mixture was heated in a microwave until all the solid agarose was dissolved in TAE buffer. The solution was allowed to cool for 3 to 4 minutes before pouring into a gel box. Ethidium bromide (0.8 µl/mL) was added to the gel mixture for staining purposes. The prepared gel solution was poured into a gel box and allowed to solidify. A mixture of 2 uL 6X blue-orange loading dye and a 10-uL DNA sample was injected into the wells (Hartwell et al., 2004). A DNA

ladder containing 40 ng/μL Lambda (λ) DNA, HindIII cut and 30 ng/μL phi X174 (□) DNA, HaeIII cut was used as a marker. The DNA was electrophoresed under a 100-volt potential difference across the gel for one hour. Finally, migrated DNA on the gel was viewed and photographed under ultraviolet light using a bioimaging system (GDS-8000, UVP Inc. Upland, CA).

2.2.2.3 Polymerase Chain Reaction (PCR)

PCR was performed on the extracted DNA sample using EconoTaq® PLUS 2X Master Mix, which includes the Taq polymerase (Lucigen Corporation, Middleton, WI). Forward and reverse primers (0.1 μM of each) were added to target the *mcrA* gene. Nuclease-free H₂O was used to make a 100-μL reaction volume. The primers used for the first PCR and a second, nested PCR amplification to obtain GC clamp products for DGGE of the *mcrA* gene are described in Table 2.1

Table 2.1: Primers to be used in PCR reactions

Gene	F/R	Primer's Labels	References
<i>mcrA</i>	Forward	<i>mcrA</i> 1f (5' - *GC-clamp- GGTGGTGTMGGA TTCACACARTAYGCWACAGC -3')	Luton et al., 2002
	Reversed	<i>McrA</i> 500r (5' – TTCATTGCRTAGTTWGGRTAGTT – 3')	

* GC-clamp = 5' – CGCCGCGCGCGCCCGCGCCGTGCCGCGCCCCCGCCG – 3'

PCR was completed using a thermal cycler (Bio-Rad PTC-200 DNA Engine, Hercules, California). Both first PCR and nested PCR required a three-step thermocycler programme in series including denature, anneal and extend. The first PCR program included denature step (95°C for 5 min), anneal step (35 cycles of 95°C for 1 min, 49°C for 1 min and 72°C for 3 min) and extend step (72°C for 7 min). The nested PCR

program included denature step (95°C for 5 min), anneal step (40 cycles of 95°C for 1 min, 58°C for 1 min and 72°C for 3 min) and extend step (72°C for 7 min) as described by others (Tale, 2010).

2.2.2.4 PCR purification

For DGGE, samples were cleaned using the UltraClean™ PCR Clean-up™ Kit (MoBio Laboratories, Carlsbad, CA). This clean-up step was employed in an effort to remove unwanted reaction components.

2.2.2.5 Denaturing Gradient Gel Electrophoresis (DGGE)

DGGE was performed on a 1-mm-thick 8 % polyacrylamide gel prepared per the manufacturer's protocol (Tale, 2010). Urea and formamide were used as denaturing reagents. Gels with a linear gradient of 40% denaturant concentration at the top of the gel and 80% at the bottom (expressed as v/v of the total gel) were used for electrophoresis. The highest and the lowest concentrations of the denaturant were 75 mm apart. A BioRad Universal DCode Mutation Detection System was used to produce the DGGE gels. The purified PCR product (1.05 µg, 35 µL) was added to each lane of the polyacrylamide gel with 7 mL of 6X loading dye. An electric potential of 100 V was applied across the gel for 12 hours. A 1 % solution of SYBR® Gold Nucleic Acid stain (Invitrogen, CA USA) dye was used for gel staining. The gel was immersed in the staining solution and rotated on a gyratory shaker table at 1 rpm for 30 min before observing it under ultra violet light using a bioimaging system (GDS-8000, UVP Inc. Upland, CA).

2.2.2.6 DGGE image analysis

The stained DGGE gel was visualized under ultraviolet light and its image was taken using a digital camera. The Lab Works software (v. 4.6.00.0) was used for detecting bands and measuring band optical density. Parameters used for band detection are presented in Table 2.2.

Table 2.2: Parameters used for bands detection

Parameter	Values
Minimum band height	0.05
Dark bands and bright background	On
Rows of equal molecular weight	On
Allowed error (%)	5
Maximum OD level for the image	On
Number of largest bands retained	5
Center peak	On

A common amplified DNA (mcrA) sample was prepared by mixing the amplified DNA samples from three digesters (R1, R3 and R5). This mix was used as a ladder/marker (L) for comparing densitometric data from two gel images. The ratio between the densitometric data (optical densities) from the marker lanes of the first and the second gel images was used to normalize the densitometric data of the second gel.

2.2.2.7 Cluster analysis

Pearson's correlation coefficients were calculated between lanes containing banding patterns obtained from DGGE gels to make dendrograms showing differences among banding patterns (Griffiths et al., 2000; Zhang and Fang, 2000; Kosman and Leonard, 2005). This coefficient measures the similarity between the two lanes

containing banding patterns. Each lane represented a specific digester biomass sample. Dissimilarities/distances between the lanes were calculated as one minus Pearson's correlation coefficient. The distance matrix was constructed using obtained dissimilarities/distances between lanes. It consisted of 6 rows and 6 columns representing each digester biomass sample. The distance matrix was used to make a dendrogram using the Phylogeny Inference Package (PHYLIP, v 3.68) selecting the unweighted pair group method with arithmetic mean (UPGMA) algorithm for clustering.

Principal component analysis (PCA) was performed on the densitometric data using the MATLAB (v.7.12(R20011a)) software package. Band intensities were used as input. A graph of the first versus the second principal component was plotted in which each biomass sample represented a data point. Some samples were clustered into groups using their first two principal components by the farthest neighbor algorithm. Equations for first and second principal components are described below:

$$\text{Component 1} = \sum_{m=1}^r \alpha_m X_m$$

$$\text{Component 2} = \sum_{m=1}^r \beta_m X_m$$

Where

α and β are first and second principal components coefficients, respectively

r: total number of bands

m: band number

$$X_m = I_m - \frac{\sum_{i=1}^n I_{m,i}}{n}$$

X_m : Demeaned optical band intensity of m^{th} band for particular reactor

I_m : Optical band intensity of m^{th} band for particular reactor

$I_{m,i}$: Optical band intensity of m^{th} band and i^{th} reactor

i= reactor number

n: total number of reactors

2.2.2.8 PCR and Cloning of excised bands

PCA was also used to identify bands of interest which had the most significant effect on the clustering. A given significant band was excised from three different lanes of the DGGE gel (the Control, Co-digester 1 and Co-digester 2 sample lanes). The excised DNA bands were immediately eluted with 100 μ L of water and kept at 4°C for 2 days to allow DNA in the gel to diffuse into water. The DNA was amplified with both forward and reversed primers, *mcrA*1f and *McrA*500r, using the protocol described in the section 2.2.2.3. However, only the first PCR step was conducted for targeting *mcrA* genes. These PCR products were run on an agarose gel to confirm presence of amplified DNA as described in section 2.2.2.2. The amplified products were cloned into One Shot® Mach1™-T1^R chemically competent *E. coli* cells using the TOPO TA Cloning® Kit according to the manufacturer's instructions (Invitrogen, Carlsbad, CA). The Chemically competent *E. coli* cells were inoculated to petri dishes containing S-Gal™/Kanamycin/LB Agar blend (Sigma-Aldrich, St. Louis, MO) and 50 mg/mL ampicillin. Twelve white/light colored colonies containing plasmids with amplified product were picked for each band and directly PCR amplified with PucF (5'-GGA ATT GTG AGC GGA TAA CA- 3') and PucR (5'- GGC GAT TAA GTT GGG TAA CG - 3') primers. The PCR was performed using EconoTaq® PLUS 2X Master Mix, which includes the Taq polymerase (Lucigen Corporation, Middleton, WI). Forward and reverse primers (0.1 μ M of each) were added to target the *mcrA* gene. Nuclease-free H₂O was used to make a 100- μ L reaction volume. PCR was completed using a thermal cycler (Bio-Rad PTC-200 DNA Engine, Hercules, California) using a thermocycler programme including denature, anneal and extend periods. The PCR program included denature step

(94°C for 2 min), anneal step (30 cycles of 94°C for 1 min, 55°C for 1 min and 72°C for 1 min) and extend step (72°C for 10 min). These PCR products were run on an agarose gel to confirm presence of amplified DNA as described in section 2.2.2.2.

2.2.2.9 PCR purification

Amplified samples were cleaned using the UltraClean™ PCR Clean-up™ Kit (MoBio Laboratories, Carlsbad, CA) according to manufacturer's instructions to remove unwanted reaction components.

2.2.2.10 Sequencing and sequence reads analysis

The purified and amplified products were sequenced at the DNA sequencing facility, University of Chicago Cancer Research Center using an Applied Biosystems 3730XL 96-capillary system. The forward and reversed sequencing reactions were performed using primers M13for 5' GTAAAACGACGGCCAGT 3' and M13rev 5' CACACAGGAAACAGCTAT GACCAT 3' respectively. A tailor-made computer program was used to clean raw sequences, form contigs, create fasta files, remove vectors and orient sequences. This program utilized the UniVec Database of the National Center for Biotechnology Information (NCBI) using the Basic Local Alignment Search Tools (BLAST) to remove vector sequences (Altschul et al., 1997). The complete cleaned sequences were submitted to NCBI database as query to identify similar *mcrA* gene sequences using the BLASTn algorithm/program.

2.3 Results and Discussion

2.3.1 Performance of bench scale-co-digestion with most promising wastes

Bench scale performance results are adapted from Navaneethan et al. (2011), and are summarized in Table 2.3. CH₄ production rates of Co-Digestion 1 and 2 systems increased by 105% and 66% in comparison to the Control systems. The extra CH₄ production from the additional co-digestates was theoretically anticipated to be 57% and 23% greater for Co-Digester 1 and 2 systems, respectively. Co-digestion of promising co-digestates in addition to the primary sludge resulted in an additional CH₄ production of 0.5 L/day. Therefore, co-digestion resulted in synergism. Moreover, TS and VS removal in Co-Digestion 1 and 2 systems increased by 50% and 33%, respectively, in comparison to the control systems.

Table 2.3: Operational and steady performance characteristics after co-digestion

Parameters	Control	Co-digester 1	Co-digester 2
SRT (days)	15	15	15
Organic loading rate (g VS/L-day)	1.6	2.2	1.9
Actual CH ₄ (L/day)	1.3	2.7	2.2
Theoretical CH ₄ from co-digestates ¹ (L/day)	0	0.9	0.4
Theoretical total CH ₄ (L/day)	1.3	2.2	1.7
Additional CH ₄ from synergism (L/day)	0	0.5	0.5
TS reduction (%)	46	73	61
VS reduction (%)	59	88	78
Biogas CH ₄ content (%)	61	62	62

¹Theoretical CH₄ from co-digestates was calculated from BMP values of respective wastes and COD added

2.3.2 Specific methanogenic activity (SMA) of biomass

The SMA values of biomass from each of the six bench-scale digesters were calculated from triplicate assays. The SMAs for the duplicate digesters in each system were not statistically different. Therefore, all six SMA measurements for each system were averaged. The SMAs against each substrate (acetate, propionate and hydrogen) are described below.

2.3.2.1 SMA against acetate and propionate

The SMAs against acetate as a substrate are presented in Figure 2.1. Error bars represent the standard deviation of the six SMAs for each system. The highest SMA values were obtained for the biomass taken from the Co-Digester 1 systems, whereas Co-Digester 2 biomass also demonstrated SMA values higher than the Control systems. The increases in average SMA value of the biomass due to co-digestion were 19 ± 9 % and 18 ± 9 % for Co-Digester 1 and 2 systems, respectively, compared to the Control systems. The SMAs were statistically different at the 99% significance level between Control and Co-Digester 1 ($F(1, 10) = 31$ and $\alpha < 0.001$) as well as Control and Co-Digester 2 ($F(1, 10) = 28.9$ and $\alpha < 0.001$).

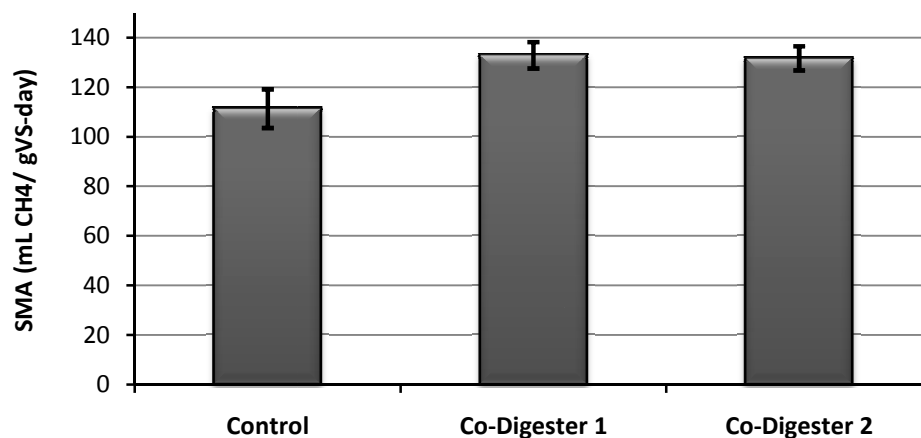


Figure 2.1: SMA results against acetate of the different conditions

The SMAs against propionate as a substrate are presented in Figure 2.2. Error bars represent the standard deviation of the six SMAs for each condition. Higher SMAs were obtained for the biomass taken from Co-Digester 1 and 2 systems. The increases in SMAs of the biomass due to co-digestion were 27 ± 12 % and 32 ± 16 % for the Co-Digester 1 and 2 systems, respectively, compared to the control. The average SMA values were statistically different at the 99% significance level between Control and Co-Digester 1 ($F(1, 10) = 31.8$ and $\alpha < 0.001$) as well as Control and Co-Digester 2 ($F(1, 10) = 26.6$ and $\alpha < 0.001$).

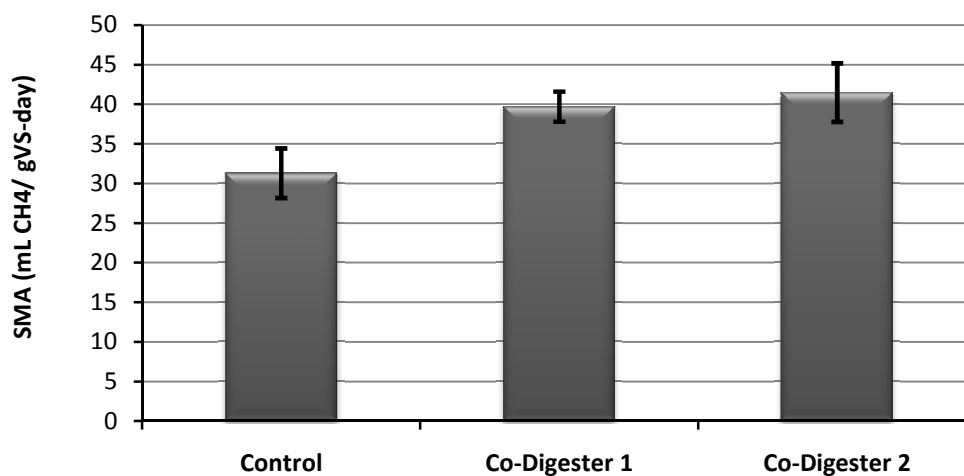


Figure 2.2: SMA results against propionate of the different conditions

2.3.2.2 SMA against H₂

The SMAs against H₂ as a substrate are presented in Figure 2.3. Error bars represent standard deviation of the six SMAs for each condition. The higher SMAs were obtained for the biomass taken from the Co-Digester 1 and 2 systems. The increases in SMA values of the biomass due to co-digestion were 36 ± 19 % and 15 ± 25 % for Co-Digester 1 and 2 systems, respectively, compared to the Control. The SMAs were statistically different at the 99% significance level between Control and Co-Digester 1 systems ($F(1, 10) = 22.5$ and $\alpha = 0.001$), whereas the SMAs were not statistically different at the 95% significance level between the Control and Co-Digester 2 systems ($F(1, 10) = 2.3$ and $\alpha = 0.16$).

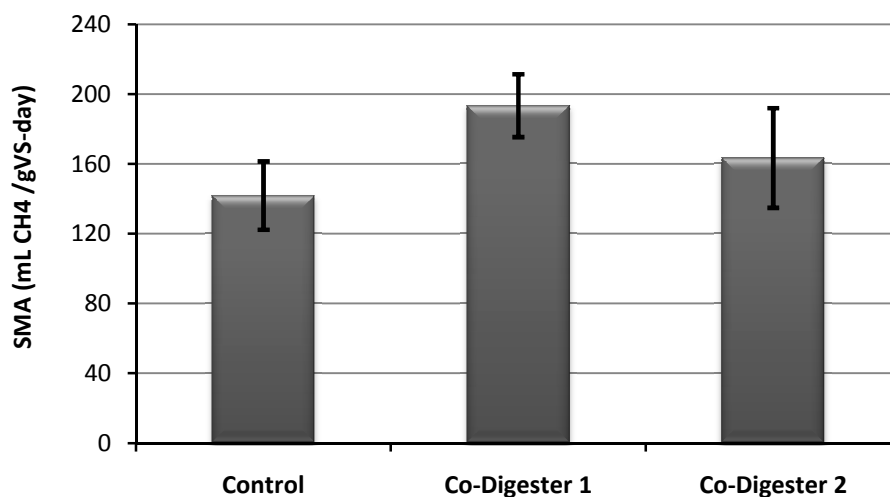


Figure 2.3: SMA results against H₂ of the biomass from the different digesters

For all three substrates, acetate, propionate and H₂, the SMAs of biomass in the co-digesters increased compared to that of the controls. The reasons for increased SMAs may be either an increase in the total number of microbes present in co-digesters (but the same general microbial community structure), the establishment of a new microbial

community structure in co-digesters, or both. The microbial community structures in different digesters were compared using molecular techniques as described below.

2.3.3 Influence of co-digestion on microbial community structure

2.3.3.1 DGGE images of *mcrA*

DGGE banding patterns for the *mcrA* functional gene before co-digestion (a) and 8 weeks (>3 SRTs) after the start of co-digestion (b) are shown in Figure 2.4. In addition, the banding pattern 2 weeks after co-digestion is shown in Figure B.1 of Appendix B. Five major bands were detected based on the preset parameters presented in Table 2.2. Densitometric data (optical band intensities) extracted from banding patterns of DGGE images 2 and 8 weeks after the beginning of co-digestion are presented in Table B.1 of Appendix B. One band (B5) was not present before co-digestion, but appeared on all lanes (except marker lane) 2 and 8 weeks after the start of co-digestion (see Figure 2.4 and Figure B.1 of Appendix B).

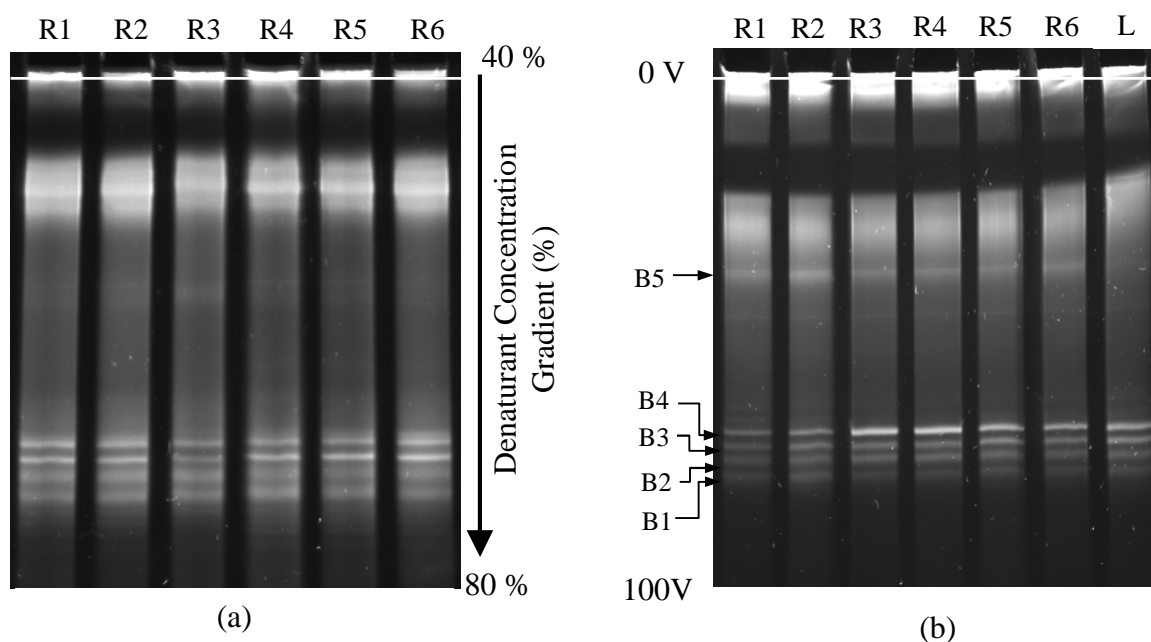


Figure 2.4: DGGE image (a) Before co-digestion and (b) at 8 weeks after co-digestion

2.3.3.2 Dendrogram of *mcrA* of biomass from digesters

The dendrograms obtained from banding patterns of DGGE images 2 and 8 weeks after the beginning of co-digestion are presented in Figure 2.5-2.6. The distance between each pair of samples was calculated as one minus the correlation coefficient between densitometric data (band intensities) of the two samples. The biomass samples from Reactors 1 and 2 clustered at 2 and 8 weeks after the beginning of co-digestion. This indicated that methanogenic microbial communities in the duplicate control digesters were similar. At 8 weeks (more than 3 SRTs) after co-digestion, the biomass samples from the duplicate digesters for each condition clustered together (see Figure 2.6). Microbial communities in the Control (Reactors 1 and 2); Co-Digester 1 (Reactors 3 and 4) and Co-Digester 2 (Reactors 5 and 6) systems were different 3 SRTs after the beginning of co-digestion.

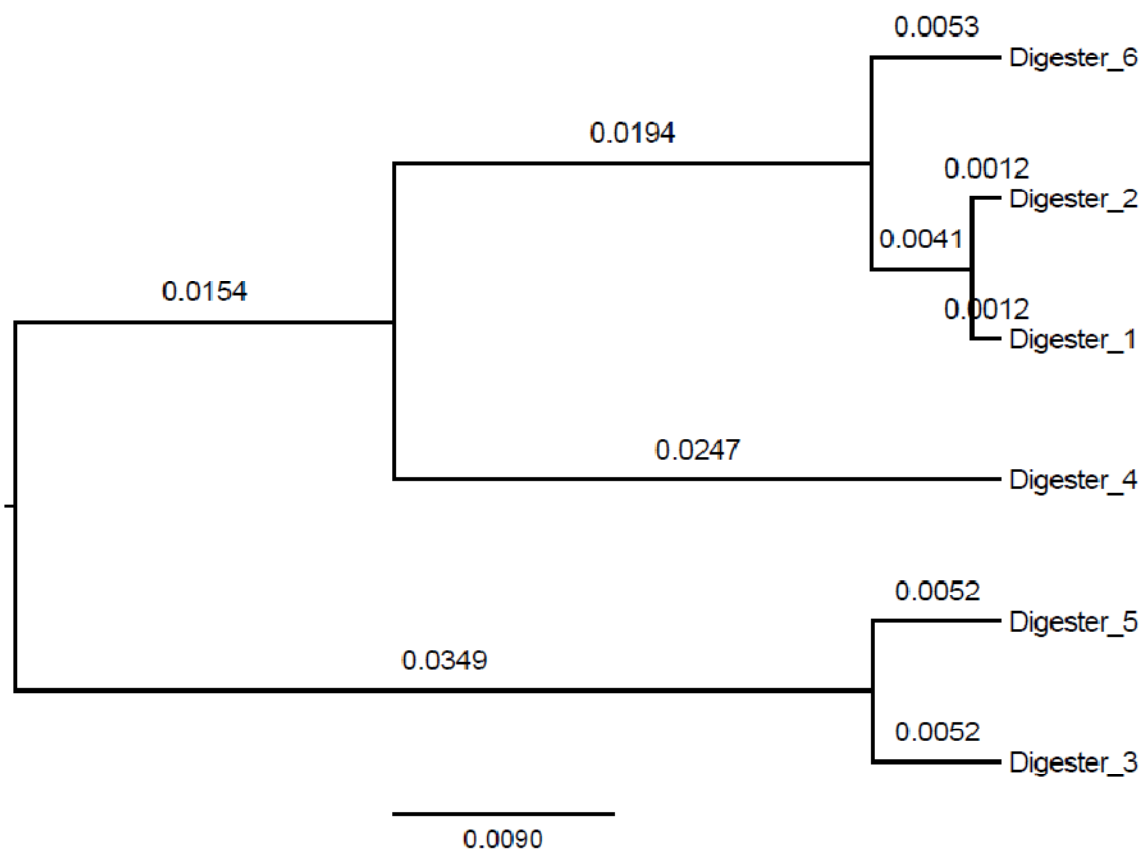


Figure 2.5: Cluster analysis of the samples at 2 weeks after co-digestion

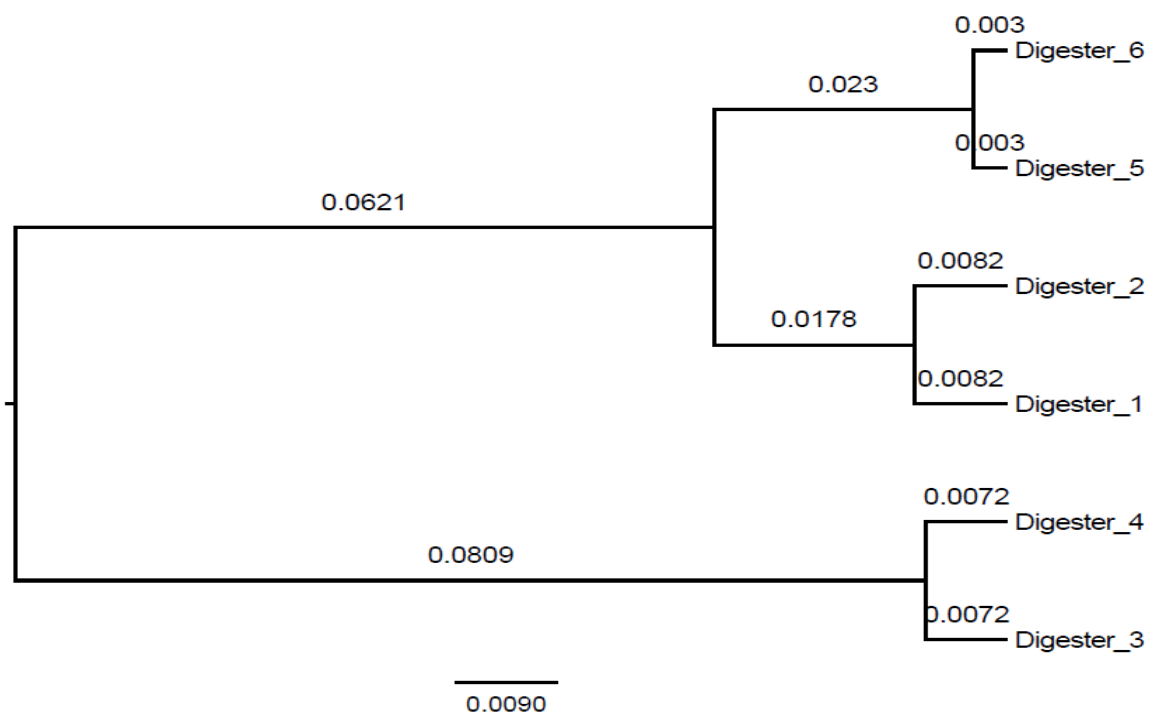


Figure 2.6: Cluster analysis of the samples at 8 weeks after co-digestion

2.3.3.3 Principal component analysis (PCA)

The principal component analysis of densistometric data (band intensities) of each biomass sample at 2 and 8 weeks after beginning of co-digestion is presented in Figures 2.7 – 2.8. Each data point in the plot represents the biomass sample of one digester. In this plot, the first and second principal components are denoted on the x-axis and y-axis, respectively. PCA analysis and dendrogram cluster analysis resulted in similar findings.

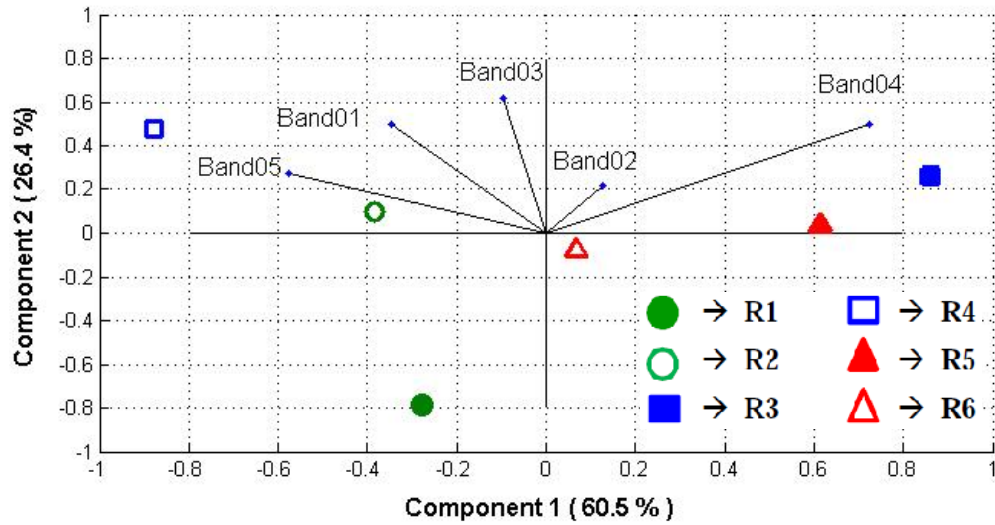


Figure 2.7: Principal component analysis results at 2 weeks after co-digestion
 Component 1 = $-0.3469(X_1) + 0.1275(X_2) + 0.0962(X_3) + 0.7222(X_4) - 0.5767(X_5)$
 Component 2 = $0.4985(X_1) + 0.2150(X_2) + 0.6169(X_3) + 0.5007(X_4) + 0.2719(X_5)$
 Where X_m : Demeaned optical band intensity of m^{th} band for particular reactor (see method Section 2.2.2.7)

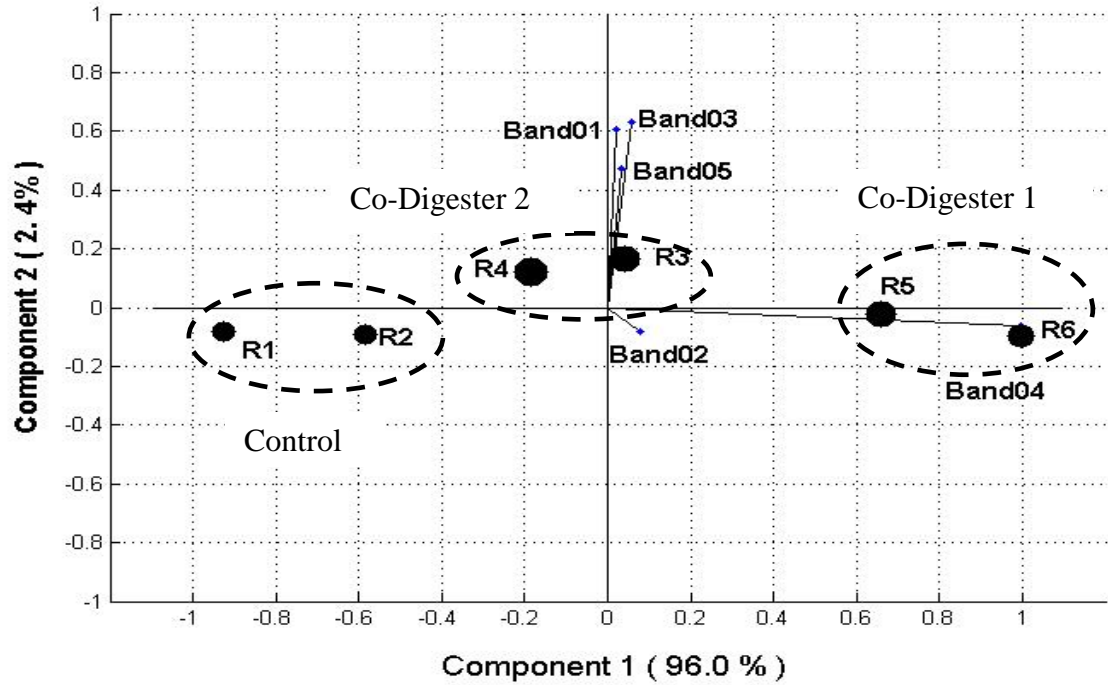


Figure 2.8: Principal component analysis results at 8 weeks after co-digestion

$$\text{Component 1} = 0.0217(X_1) + 0.0765(X_2) + 0.0595(X_3) + 0.9946(X_4) + 0.0311(X_5)$$

$$\text{Component 2} = 0.6082(X_1) - 0.0813(X_2) + 0.6314(X_3) - 0.0595(X_4) + 0.4705(X_5)$$

Where X_m : Demeaned optical band intensity of m^{th} band for particular reactor (see method Section 2.2.2.7)

In the PCA at 8 weeks after the beginning of co-digestion (Figure 2.8), the first principal component explained 96% of the total variation for densitometric data. The size of the circle symbols in Figure 2.8 represents the relative values of SMA against H₂, i.e. larger circles denote higher SMA values. Points (biomass) in the plot (see Figure 2.8) were clustered into 3 groups representing three different conditions, Control, Co-Digester 1 and Co-Digester 2 systems, using nearest neighbor algorithm. The three conditions were different based on methanogenic microbial community structures. The different specific methanogenic activities (SMAs) obtained among the three conditions may be explained by these changes in methanogenic microbial structure, since microbial community structure affects the rate and extent of CH₄ production (Tale et al., 2011).

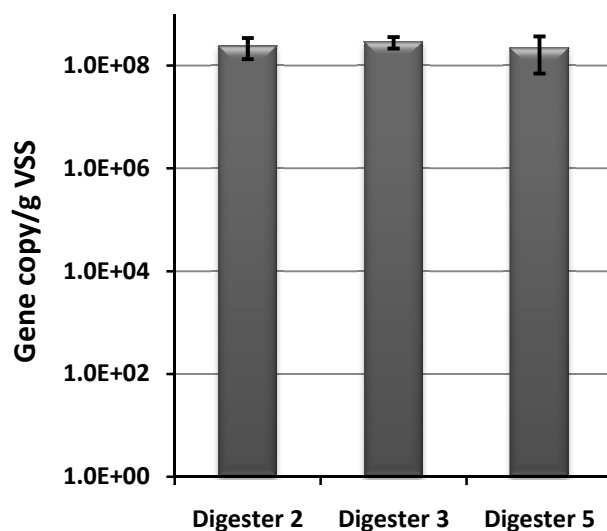
Each of the five variables (B1-B5) was represented in this plot by a vector, and the direction and length of the vector indicated how each band contributed to the two principal components. Therefore, Band 4 (long length) was a major contributor for partitioning the biomass samples into three clusters. Moreover, the direction of Band 4 was toward the Co-Digester 1 cluster. The organism(s) represented by Band 4 ostensibly play a more significant role in Co-Digester 1 systems than others (Control and Co-Digester 2). After Band 4, Band 2 and 3 were major contributors to the principal components (see Figure 2.8). Overall, performance of the Co-Digester 1 systems was correlated to the intensity of Band 4. This indicated that organisms represented by this band may have a significant metabolic function leading to higher SMAs in the system co-digesting synergistic wastes.

Clones extracted from the most significant DGGE band (Band 4) shared a 90-99% sequence similarity to *Methanospirillum hungatei*. Steinbery and Regan (2008) suggested that gene sequence similarities more than 88.9% and 79% could be considered to be within the genus and family levels, respectively. Therefore, the excised band was similar to *Methanospirillum hungatei* at the genus level. Cleaned sequences from clones were deposited in the GenBank database.

2.3.4 quantitative polymerase chain reaction (qPCR)

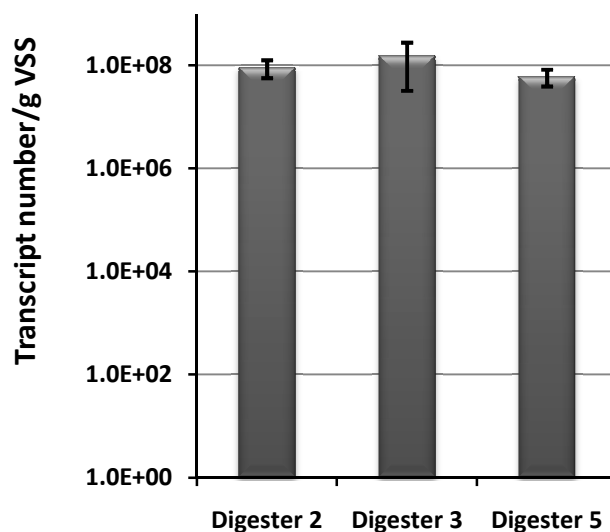
Microbial community structure was also investigated by Morris (2011) using qPCR with *mcrA* specific primers and DNA as well as cDNA from Digesters 2, 3 and 5. Quantitative polymerase chain reaction was performed on the biomass samples in tandem

with SMA measurements. The *mcrA* gene copy per g VSS and transcript numbers per g VSS for Digester 2 (one of the Control systems), Digester 3 (one of the Co-Digester 1 systems) and Digester 5 (one of the Co-Digester 2 systems) are presented in Figures 2.9 (a) and (b), respectively. Error bars represent standard deviation of triplicate measurements. The gene copy and transcript numbers for total *mcrA* were not statistically different among the digesters at a confidence level of 95% (see Table B.2 and Appendix B). However, gene copy and transcript numbers for specific *mcrA* subgroups may be different or the same. Based on results from PCA analysis of DGGE banding patterns, the specific *mcrA* gene (Band 4) was significantly different among the three systems and a dominant contributor to differences in methanogenic community structure.



a) *mcrA* copy number/ g VSS

Figure 2.9: Results of qPCR for the digesters (Adapted from Morris, 2011)



b) mcrA transcripts/ g VSS

Figure 2.9: Results of qPCR for the digesters (Adapted from Morris, 2011)

Total DNA, RNA and VSS concentrations in digesters are presented in Table 2.4. The DNA and RNA concentrations were approximately same among the digesters. The DNA and RNA concentration in the biomass did not positively correlate with volatile suspended solids concentration of the biomass.

Table 2.4: Total DNA, RNA and VSS in the digested biomass (Adapted from Morris, 2011)

Sample Name	Nucleic Acids (ng/L biomass)		Volatile Suspended Solids(g/L of biomass)
	DNA	RNA	
Digester 2 (Control)	1.31×10^5	7.9×10^4	8.4
Digester 3 (Co-Digester 1)	1.31×10^5	8.2×10^4	11.0
Digester 5 (Co-Digester 2)	1.31×10^5	6.8×10^4	8.4

2.3.5 Relationship between SMA and microbial community structures using DGGE and qPCR analyses

Both PCA and dendrogram analyses indicated that the methanogenic community in the co-digestion systems was different from that of the control. The different SMAs among the three conditions may be explained by changes in the microbial community structure. This microbial shift was a result of differences in gene copy/transcript numbers of sub groups of the *mcrA* gene although the total number of *mcrA* gene and transcript copies was approximately the same. In addition, higher SMAs against H_2/CO_2 in the Co-Digester 1 system may have resulted from the contribution of *Methanospirillum hungatei* represented by Band 4 in the *mcrA* DGGE analysis.

2.4 Conclusions

Co-digestion of synergistic wastes (most promising wastes) increased CH_4 production rate more than the total value of CH_4 production rate when each waste was digested alone. The co-digestion of synergistic wastes (Co-Digester 1 system) increased SMAs by 19%, 27% and 36% against acetate, propionate and H_2 as substrates, respectively. The different SMAs among three conditions were putatively due to changes in microbial community. The presence of *Methanospirillum sp* correlated to higher SMAs in the Co-Digester systems. Co-digestion of synergistic wastes can lead to changes in microbial community and more rapid maximum methane production rate through enhanced microbial activity. Therefore, co-digestion of synergistic wastes is one method to increase renewable energy by improving microbial community.

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Chapter 3

Overall Conclusions, Future Study and Recommendations

3.1 Overall conclusions

Co-digestion outcomes can be categorized as synergistic, neutral and antagonistic based on the biogas production for digestion of multiple wastes (more than one) being greater than, the same as, or less than that observed as a sum of methane production when each waste is digested alone. A selection of most promising and suitable wastes for full-scale is an important in order to produce additional methane production through synergism among blended wastes. A method/protocol to select the most promising waste for full-scale co-digestion included four steps: (1) preliminary screening (market survey), (2) waste characterization (BMP, ATA, sieve analysis, other test including analyses of a suite of metals), (3) simple economic analysis, and (4) bench-scale digester testing. Co-digestion of synergistic wastes in full-scale increased additional biogas production significantly, which can use to produce more combined heat and power (CHP) as renewable energy and also to decrease green house gas (GHG) emission.

Co-digestion of the most promising waste increased specific methanogenic activities (SMAs) against acetate, propionate and hydrogen as a substrate. The reasons for synergistic outcomes putatively relate to increased methanogenic activities as a result of a methanogen community shift. The presence of *Methanospirillum sp.* correlated to a higher methanogenic activity of Co-Digester systems. While the total number of methanogens (mcrA gene copies) and the number of mcrA transcripts did not increase

during co-digestion, the relative numbers and identity of the methanogen species present did change. Co-digestion of synergistic wastes can improve microbial community structure resulting in more rapid methane production rate. In conclusion, co-digestion is one method to increase renewable energy production and decrease GHG emission via anaerobic digestion.

3.2 Future Study and Recommendations

More research on co-digestion of industrial waste is needed to summarize findings in different categories. In addition, the number of most promising industry wastes co-digested at full scale is limited. More research is needed to identify a wider range of the most promising industrial wastes.

This study used a simple cost-benefit analysis for selecting the most promising co-digestates. The cost-benefit analysis used typical unit value/cost for CH₄ produced, GHG avoided, treatment charge, waste conveyance fees and solid handling and disposal charges. Until now, there is no national standard for these unit values in the United States. Especially unit values for GHG avoided and the treatment fee may vary greatly. Therefore, more information on these values is required.

Presently, some regional municipal wastewater treatment plants employ co-digestion programs. They have enough capacity to co-digest additional wastes. But they may not have sufficient equipment and storage tanks to handle different and complex

wastes. It is important to have enough storage capacity because waste delivery to the treatment plant may be interrupted because of limitation or failure in transportation.

There is a question as to what is the highest organic loading rate sustainable for co-digestates that can be safely added to digesters. It depends on solids retention time (SRT), digester configuration and waste characteristics. Therefore, a maximum loading for each promising co-digestate should be determined and reported for most commonly-used digester configurations with different, possible SRT values. Moreover, the optimum ratio between co-digestate and municipal sludge should be determined. This research study focused on a method to identify the most promising co-digestates rather than finding the maximum loading rate and optimum ratio between primary sludge and co-digestates.

In this research, synergistic outcomes of co-digestion were correlated to increased acetate, propionate and hydrogen specific methanogenic activities. However, more exact mechanisms for synergism should be identified and explained from a microbial point of view using molecular techniques like DGGE, cloning, sequencing or quantitative PCR.

In this study, the influence of co-digestion on methanogen community was investigated. However, four major groups work in the total anaerobic digestion process. It is important to understand how co-digestion influences bacteria (hydrolytic bacteria, fermenting bacteria, syntrophic acetogenic bacteria) as well as methanogens.

Band 2 (B2) and Band (B3) on the DGGE gel was identified by PCA as the significant contributor to synergistic outcomes of Co-Digester 2 system. Therefore, the methanogens represented by B2 and B3 should be identified by sequencing the excised band.

SMA's against acetate, propionate and H_2 increased for both co-digestion biomass communities compared to control biomass. This indicates that co-digestion influences either the quantity or activity of acetate, propionate and H_2 utilizers. It is necessary to determine how much each group individually contributes to the synergistic outcome. This could be done using quantitative PCR (qPCR) with specific primers for acetate, propionate and H_2 utilizers.

This study only focused on the influence of co-digestion on microbial communities when co-digesting synergistic wastes. It is better to compare microbial community changes/responses when co-digesting antagonistic waste as well.

In SMA calculations, biomass presented in the sample was quantified by volatile solids (VS). It may overestimate active biomass of the sample used because VS may consist of some inert VS in addition to active biomass.

Appendix

A

Table A.1: Cost-benefit analysis for promising co-digestates

	1	2	3	4	5	6
Parameters	Cookie	Float	Whole stillage	Syrup	Trube	Brewery yeast
COD (mg/L)	12,543	132,816	154,778	398,718	203,294	313,380
VS (%)	0.5	11.31	13.49	27.44	9.5	14.3
TS (%)	0.6	12.53	14.45	30.44	9.9	16.2
FOG (mg/L)	3,309	59,400	N/A	51,640	4,580	280
BMP (mlCH ₄ /gCOD or mlCH ₄ /gVS)	418	416	399	396	373	373
ATA	IC ₅₀ >50%	IC ₅₀ >10%	IC ₅₀ >10%	IC ₅₀ >4%	IC ₅₀ =1.8%	IC ₅₀ =4.7%
d50% Passing (mm)	0.2	< 0.075	0.39	< 0.053	< 0.053	< 0.053
Miles to South Shore WWTP	95.2	15.9	68.6	68.6	18.15	18.15
Shipping cost (\$/1000gal)	95.2	15.9	68.6	68.6	18.2	18.2
Soilds handling cost (\$/1000gal)	1.5	28.6	32.1	69.7	21.5	37.7
Value of biogas (\$/1000 gal)	4.2	44.3	49.5	126.6	60.8	93.7
Treatment fee (\$/1000gal)	13.6	213.4	247.0	560.6	223.2	354.5
Income from C emission credits (\$/1000gal)	0.2	1.9	2.2	5.5	2.7	4.1
Net benefit (\$/m ³)	-20.8	56.8	52.3	146.5	65.3	104.7

Table A.1: Cost-benefit analysis for promising co-digestates (continued)

	7	8	9	10	11	12	13
Parameters	Heads from rum distillation	FT reactor condensate	Pre-filter slurry	Thin stillage	Confectionary	Corn/Rye/Wheat/Barley in liquid	Flavorings yeast
COD (mg/L)	1,443,595	103,646	38,555	137,241	23,150	171,856	215,599
VS (%)	0.00	0.01	1.54	8.27	1.8	11.65	15.09
TS (%)	0.00	0.01	1.67	9.12	1.9	11.93	15.71
FOG (mg/L)	50	ND	710	31,370	933	ND	2,530
BMP (mlCH ₄ /gCOD or mlCH ₄ /gVS)	368	365	352	351	346	326	326
ATA	> 0.8%	> 12%	> 30%	IC ₅₀ >12%	IC ₅₀ >40%	> 8%	IC ₅₀ >5%
d50% Passing (mm)				< 0.075	< 0.053		< 0.053
Miles to South Shore WWTP	15.3	954	16.2	68.6	55.08	36	7.68
Shipping cost (\$/1000gal)	15.3	954.0	16.2	68.6	55.1	36.0	7.7
Soilds handling cost (\$/1000gal)	0.0	0.0	3.8	20.8	4.2	25.5	34.0
Value of biogas (\$/1000 gal)	425.6	30.3	10.9	38.6	6.4	45.0	56.4
Treatment fee (\$/1000gal)	800.8	57.6	40.1	177.8	34.0	228.4	294.8
Income from C emission credits (\$/1000gal)	18.6	1.3	0.5	1.7	0.3	2.0	2.5
Net benefit (\$/m ³)	324.9	-228.5	8.3	34.0	-4.9	56.5	82.4

Table A.1: Cost-benefit analysis for promising co-digestates (continued)

	14	15	16	17	18	19	20
Parameters	Can crushing waste	Acid whey	Yeast centrate	Sorghum	Molasses wash	Oil and hydraulic fluids	Metal Cutting
COD (mg/L)	76,431	147,990	35,479	89,038	125,661	76,875	75,351
VS (%)	5.60	10.75	0.57	4.78	6.47	2.37	2.23
TS (%)	6.10	12.70	0.59	5.57	9.33	2.60	2.29
FOG (mg/L)	442	748	4,465	380	3300	7,350	32,150
BMP (mlCH ₄ /gCOD or mlCH ₄ /gVS)	325	295	285	260	251	79	65
ATA	IC50>30%	IC50>8%	IC50>30%	> 12%	> 8%	IC50>15%	IC50 = 12.5%
d50% Passing (mm)	< 0.053	< 0.053	< 0.053			< 0.053	< 0.053
Miles to South Shore WWTP	74.5	49	7.68	35	15.3	12.5	29.6
Shipping cost (\$/1000gal)	74.5	49.0	7.7	35.0	15.3	12.5	29.6
Soilds handling cost (\$/1000gal)	13.8	30.5	1.3	13.2	25.4	5.9	4.9
Value of biogas (\$/1000 gal)	19.9	35.0	8.1	18.5	25.3	4.9	3.9
Treatment fee (\$/1000gal)	110.4	223.7	26.3	111.5	173.8	71.6	67.4
Income from C emission credits (\$/1000gal)	0.9	1.5	0.4	0.8	1.1	0.2	0.2
Net benefit (\$/m ³)	11.4	47.8	6.8	21.8	42.1	15.4	9.8

Table A.1: Cost-benefit analysis for promising co-digestates (continued)

	21	22	23	24	25	26	27
Parameters	Soap	Boiler Cleaning	Mustard waste	Pine apple	Alage (Botryococcus braunii)	Wet distillers grain	Waste noodle
COD (mg/L)	47,299	32,906	58,698	94,061	1,749,000	206,243	502,416
VS (%)	1.2	4.80	8.53	6.52	91.52	31.14	35.29
TS (%)	2	5.75	9.21	6.97	98.67	32.94	36.21
FOG (mg/L)	4,837	-	5,320	5822*	-	N/A	N/A
BMP (mlCH ₄ /gCOD or mlCH ₄ /gVS)	20	20	580	516	500	473	453
ATA	IC50=2%	IC50 = 9.5 %	IC50 = 14.4%	> 15%	> 0.8%	IC50>6%	IC50>3%
d50% Passing (mm)	< 0.053	< 0.053	1.27			0.47	> 4.75
Miles to South Shore WWTP	17.8	30	32.9	15.2	15	68.6	61
Shipping cost (\$/1000gal)	17.8	30.0	32.9	15.2	15.0	68.6	61.0
Soilds handling cost (\$/1000gal)	5.8	14.0	20.6	15.5	220.5	72.4	77.3
Value of biogas (\$/1000 gal)	0.8	0.5	39.69	27.02	367.27	118.23	128.29
Treatment fee (\$/1000gal)	48.5	82.4	135.3	130.0	2072.1	481.9	682.9
Income from C emission credits (\$/1000gal)	0.0	0.0	1.2	1.7	30.6	3.4	8.0
Net benefit (\$/m ³)	6.8	10.3	32.4	33.8	590.4	122.2	179.9

Table A.1: Cost-benefit analysis for promising co-digestates (continued)

	28	29	30	31	32	33	34
Parameters	Waste rice	Cabbage	Corn Stover	Alage (Nannochloropsis)	Sprout	Brewery Grain	Cooking solids
COD (mg/L)	286,867	49,957	1,662,265	1,413,000	127,243	107,377	1,056,489
VS (%)	22.69	4.34	80.76	87.71	14.33	20.1	44.63
TS (%)	22.98	4.76	90.30	96.81	15.00	21.4	46.76
FOG (mg/L)	N/A	155	110	-	N/A	N/A	650
BMP (mlCH ₄ /gCOD or mlCH ₄ /gVS)	414	412	396	394	389	367	366
ATA	IC50>6%	> 25%	> 0.8%	> 0.8%	IC50>10%	IC50>10%	> 1%
d50% Passing (mm)	> 4.75				> 0.25	1.17	
Miles to South Shore WWTP	61	15.2	100	15	7.68	18.15	6.2
Shipping cost (\$/1000gal)	61.0	15.2	100.0	15.0	7.7	18.2	6.2
Soilds handling cost (\$/1000gal)	48.5	10.8	208.0	220.6	32.6	47.3	101.9
Value of biogas (\$/1000 gal)	75.40	14.36	256.95	277.36	44.74	59.21	131.23
Treatment fee (\$/1000gal)	415.7	80.9	1930.6	1864.7	238.0	298.3	1108.4
Income from C emission credits (\$/1000gal)	4.2	0.7	23.0	19.5	1.7	1.4	13.5
Net benefit (\$/m ³)	101.9	18.5	502.7	508.8	64.5	77.5	302.5

Table A.1: Cost-benefit analysis for promising co-digestates (continued)

	35	36	37	38	39	40	41
Parameters	Corrigated cardboard	Lettuce	White waste	Packaging	Potatoes	Dewatered paper mill sludge	Cheese waste
COD (mg/L)	1,184,432	49,554	1,089,391	972,083	125,952	311,115	438,005
VS (%)	89.83	3.66	90.1	76.8	13.89	16.96	68.01
TS (%)	92.57	4.07	91.1	89.1	14.74	35.55	72.09
FOG (mg/L)	8*	325*	21	18	220	ND	272000
BMP (mlCH ₄ /gCOD or mlCH ₄ /gVS)	347	328	306	301	282	254	241
ATA	0.011	0.25	IC50>1%	IC50>1%	> 10%	> 3%	> 3%
d50% Passing (mm)			> 4.75	> 4.75			
Miles to South Shore WWTP	18.7	15.2	43.95	43.95	15.2	97	65.7
Shipping cost (\$/1000gal)	18.7	15.2	44.0	44.0	15.2	97.0	65.7
Soilds handling cost (\$/1000gal)	198.6	9.3	191.9	211.3	32.5	112.8	158.7
Value of biogas (\$/1000 gal)	250.54	9.63	221.28	185.54	31.47	34.60	131.45
Treatment fee (\$/1000gal)	1690.4	72.9	1621.2	1533.7	234.4	569.3	1047.3
Income from C emission credits (\$/1000gal)	14.4	0.6	11.7	10.2	1.2	2.8	3.7
Net benefit (\$/m ³)	459.2	15.5	427.6	389.5	58.0	104.9	253.1

Table A.1: Cost-benefit analysis for promising co-digestates (continued)

	42	43	44	45	46
Parameters	Paunch	Wood chip/Charcoal	Dried manure	Cocoa husks	Composting
COD (mg/L)	104,847	659,947	449,369	350,149	174,092
VS (%)	10.56	37.85	86.42	27.21	16.19
TS (%)	13.04	39.56	92.86	64.10	56.76
FOG (mg/L)	N/A	210	N/A	595	450
BMP (mlCH ₄ /gCOD or mlCH ₄ /gVS)	237	60	51	49	39
ATA	IC ₅₀ >10%	> 1.6%	IC ₅₀ >3%	> 3%	> 6%
d50% Passing (mm)	1.1		2.26		
Miles to South Shore WWTP	15.9	6.2	15.9	30	13.1
Shipping cost (\$/1000gal)	15.9	6.2	15.9	30.0	13.1
Soilds handling cost (\$/1000gal)	32.3	86.0	206.9	210.4	202.8
Value of biogas (\$/1000 gal)	20.09	18.20	35.37	10.72	5.04
Treatment fee (\$/1000gal)	203.7	807.8	1285.2	909.4	729.8
Income from C emission credits (\$/1000gal)	0.9	1.4	0.8	0.6	0.2
Net benefit (\$/m ³)	46.6	194.2	290.3	179.7	137.2

Table A.2: Biogas and co-digestates flow rate for full-scale testing

		Gas Production-KCF	Biogas 7 days moving average	Methane 7 days moving average	Co-digestate flowrate
Date	Days	KCF/day	KCF/day	m3/day	L/min
4/28/2010	5	593	593	9134	0.0
4/29/2010	6	619	619	9538	0.0
4/30/2010	7	532	532	8197	0.0
5/1/2010	8	503	503	7374	0.0
5/2/2010	9	586	586	8591	0.0
5/3/2010	10	592	592	8685	0.0
5/4/2010	11	485	559	8193	0.0
5/5/2010	12	499	545	7997	0.0
5/6/2010	13	479	525	7703	0.0
5/7/2010	14	507	522	7651	0.0
5/8/2010	15	547	528	7863	0.0
5/9/2010	16	532	520	7749	0.0
5/10/2010	17	496	507	7545	0.0
5/11/2010	18	448	501	7464	0.0
5/12/2010	19	524	505	7518	0.0
5/13/2010	20	618	525	7814	0.0
5/14/2010	21	661	547	8141	0.0
5/15/2010	22	497	539	8310	0.0
5/16/2010	23	376	517	7966	0.0
5/17/2010	24	371	499	7692	0.0
5/18/2010	25	411	494	7611	0.0
5/19/2010	26	485	488	7525	0.0
5/20/2010	27	570	482	7420	0.0
5/21/2010	28	646	480	7387	0.0
5/22/2010	29	679	505	8416	0.0
5/23/2010	30	699	552	9185	0.0
5/24/2010	31	675	595	9907	0.0
5/25/2010	32	559	616	10261	0.0
5/26/2010	33	504	619	10306	0.0
5/27/2010	34	522	612	10192	0.0
5/28/2010	35	453	585	9733	0.0
5/29/2010	36	467	554	9230	0.0
5/30/2010	37	542	532	8857	0.0
5/31/2010	38	621	524	7868	0.0
6/1/2010	39	645	537	8052	0.0
6/2/2010	40	653	558	8372	0.0
6/3/2010	41	620	572	8581	0.0
6/4/2010	42	616	595	8929	0.0
6/5/2010	43	614	616	10361	0.0
6/6/2010	44	593	623	10483	0.0
6/7/2010	45	550	613	10312	0.0
6/8/2010	46	537	598	10053	0.0
6/9/2010	47	522	579	9738	0.0
6/10/2010	48	566	571	9609	0.0
6/11/2010	49	546	561	9442	0.0
6/12/2010	50	555	553	9080	0.0
6/13/2010	51	591	552	9074	0.0
6/14/2010	52	574	556	9129	0.0
6/15/2010	53	522	554	9094	0.0
6/16/2010	54	485	548	9007	0.0
6/17/2010	55	528	543	8917	0.0
6/18/2010	56	556	544	8940	0.0
6/19/2010	57	561	545	8490	0.0
6/20/2010	58	513	534	8317	0.0
6/21/2010	59	527	527	8213	0.0
6/22/2010	60	522	527	8213	0.0
6/23/2010	61	597	543	8463	5.9
6/24/2010	62	617	556	8661	12.7
6/25/2010	63	515	550	8571	17.1
6/26/2010	64	511	543	9107	14.9

6/27/2010	65	509	543	9097	13.9
6/28/2010	66	534	544	9113	14.1
6/29/2010	67	487	539	9030	14.0
6/30/2010	68	562	534	8947	13.9
7/1/2010	69	490	516	8644	13.0
7/2/2010	70	539	519	8699	6.4
7/3/2010	71	512	519	8614	0.0
7/4/2010	72	446	510	8465	0.0
7/5/2010	73	478	502	8332	0.0
7/6/2010	74	483	501	8321	13.3
7/7/2010	75	511	494	8199	18.5
7/8/2010	76	618	512	8501	18.2
7/9/2010	77	669	531	8810	17.5
7/10/2010	78	654	551	8927	6.4
7/11/2010	79	572	569	9220	0.0
7/12/2010	80	578	584	9452	12.9
7/13/2010	81	544	592	9593	6.9
7/14/2010	82	491	589	9547	0.0
7/15/2010	83	486	571	9242	0.0
7/16/2010	84	478	543	8800	12.9
7/17/2010	85	496	521	8433	21.2
7/18/2010	86	517	513	8529	20.5
7/19/2010	87	528	506	8410	17.3
7/20/2010	88	580	511	8496	16.3
7/21/2010	89	576	523	8698	13.6
7/22/2010	90	515	527	8767	13.5
7/23/2010	91	531	535	8894	6.1
7/24/2010	92	558	544	8404	12.7
7/25/2010	93	550	548	8477	11.6
7/26/2010	94	496	544	8406	7.4
7/27/2010	95	521	535	8276	0.0
7/28/2010	96	561	533	8241	10.9
7/29/2010	97	568	541	8359	17.2
7/30/2010	98	580	548	8467	16.9
7/31/2010	99	566	549	8950	16.3
8/1/2010	100	556	550	8964	13.4
8/2/2010	101	597	564	9199	3.3
8/3/2010	102	627	579	9446	9.4
8/4/2010	103	660	593	9677	11.2
8/5/2010	104	694	611	9971	13.4
8/6/2010	105	722	632	10301	7.7
8/7/2010	106	886	677	11392	0.0
8/8/2010	107	996	740	12450	5.9
8/9/2010	108	1017	800	13460	11.9
8/10/2010	109	1001	854	14359	9.0
8/11/2010	110	876	885	14879	9.4
8/12/2010	111	961	923	15520	6.0
8/13/2010	112	1087	975	16397	10.4
8/14/2010	113	1146	1012	17252	12.8
8/15/2010	114	1018	1015	17306	11.6
8/16/2010	115	941	1004	17121	12.1
8/17/2010	116	901	990	16878	6.6
8/18/2010	117	902	994	16940	0.0
8/19/2010	118	931	989	16867	0.0
8/20/2010	119	938	968	16505	11.3
8/21/2010	120	922	936	16012	17.8
8/22/2010	121	744	897	15342	5.7
8/23/2010	122	775	873	14936	0.0
8/24/2010	123	765	854	14604	0.0
8/25/2010	124	864	848	14512	0.0
8/26/2010	125	737	821	14037	0.0
8/27/2010	126	684	784	13417	0.0
8/28/2010	127	628	742	12447	0.0
8/29/2010	128	629	726	12171	0.0

8/30/2010	129	723	719	12046	0.0
8/31/2010	130	748	716	12006	0.0
9/1/2010	131	752	700	11738	0.0
9/2/2010	132	819	712	11935	0.0
9/3/2010	133	774	725	12150	0.0
9/4/2010	134	753	743	12238	0.0
9/5/2010	135	760	761	12546	0.0
9/6/2010	136	705	759	12503	0.0
9/7/2010	137	651	745	12274	0.0
9/8/2010	138	619	726	11961	0.0
9/9/2010	139	603	695	11453	0.0
9/10/2010	140	692	683	11260	0.0
9/11/2010	141	818	693	11572	0.0
9/12/2010	142	753	692	11556	0.0
9/13/2010	143	725	695	11605	0.0
9/14/2010	144	680	699	11674	0.0
9/15/2010	145	673	706	11802	0.0
9/16/2010	146	687	718	12001	0.0
9/17/2010	147	679	716	11969	0.0
9/18/2010	148	606	686	11608	0.0
9/19/2010	149	596	664	11229	0.0
9/20/2010	150	728	664	11235	0.0
9/21/2010	151	697	666	11276	0.0
9/22/2010	152	624	659	11158	0.0
9/23/2010	153	647	654	11063	0.0
9/24/2010	154	741	663	11213	0.0
9/25/2010	155	760	685	11555	0.0
9/26/2010	156	692	698	11788	0.0
9/27/2010	157	711	696	11749	0.0
9/28/2010	158	668	692	11679	0.0
9/29/2010	159	643	695	11724	0.0
9/30/2010	160	851	724	12216	0.0
10/1/2010	161	471	685	11564	0.0
10/2/2010	162	556	656	11036	0.0
10/3/2010	163	566	638	10733	0.0
10/4/2010	164	551	615	10348	0.0
10/5/2010	165	411	578	9729	0.0
10/6/2010	166	548	565	9500	0.0
10/7/2010	167	530	519	8729	0.0
10/8/2010	168	492	522	8780	0.0
10/9/2010	169	530	518	8659	0.0
10/10/2010	170	724	541	9035	0.0
10/11/2010	171	728	566	9459	0.0

Table A.3: Excess methane production calculation due to co-digestion synergistic outcome based on VS added to digesters

	Control	Co-digestion	Post co-digestion
Period considered (days)	60	61	50
Total primary sludge VS added (tonnes VS)	2560	2760	2130
Total CH ₄ produced (kCF)	18,800	23,400	20,000
Total CH ₄ produced (m ³)	533,000	663,000	567,000
L CH ₄ / kg VS sludge added	208		
Theoretical CH ₄ production (m ³)		572,000	443,000
Additional CH ₄ (m ³)		90,900	124,000
Total volume of co-digestate added (gal)		237,000	
Average COD of co-digestate (mg/L)		59,300	
Total COD added as co-digestate (kg)		53,200	
CH ₄ from co-digestate (m ³)		21,300	
Excess CH ₄ (m ³)		69,700	124,000

Table A.4: TS removal efficiency calculation

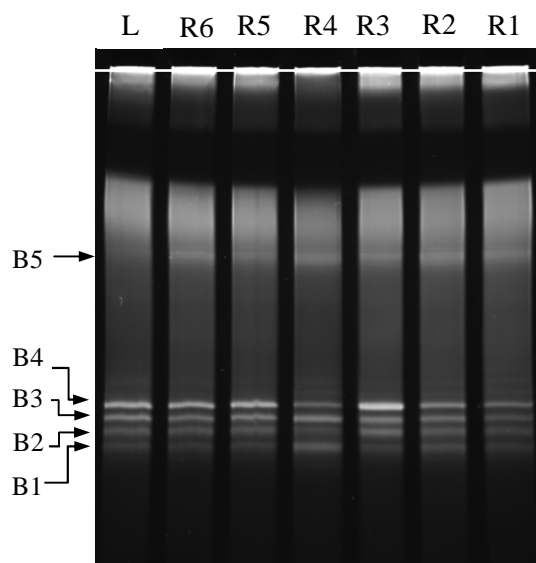
	Control	Co-digestion	Post co-digestion
Period considered (days)	60	61	50
Total primary sludge TS added (tonnes TS)	3433	4061	2776
Total co-digestate added TS (tonnes TS)	0	59	0
Total TS wasted (tonnes TS)	2462	2686	2144
TS accumulation (tonnes TS)	-45	91	-273
TS destroyed (Tonnes TS)	1016	1343	905
TS removal efficiency (%)	30	33	33

Table A.5: VS removal efficiency calculation

	Control	Co-digestion	Post co-digestion
Period considered (days)	60	61	50
Total primary sludge VS added (tonnes VS)	2563	2755	2133
Total co-digestate added VS (tonnes VS)	0	51	0
Total VS wasted (tonnes VS)	1858	1819	1431
VS accumulation (tonnes VS)	-114	45	-136
VS destroyed (Tonnes VS)	819	942	839
VS removal efficiency (%)	32	34	39

Appendix

B

Figure B.1: DGGE image at 2 weeks after co-digestion**Table B.1: Optical intensities for detected bands from DGGE gels****(a) 2 weeks after start of co-digestion**

	Band 1	Band 2	Band 3	Band 4	Band 5
L	2.3685	3.182	3.8481	5.9434	0
R6	2.0683	2.909	3.2062	4.9686	12.045
R5	2.3386	3.2107	3.6555	5.7005	10.093
R4	4.4033	2.8788	4.8294	3.3044	12.97
R3	1.9501	3.5133	3.6006	6.9526	10.7429
R2	2.5326	3.1658	3.2897	4.5075	13.479
R1	1.8335	2.4092	2.2704	2.8991	11.36

(b) 8 weeks after start of co-digestion

	Band 1	Band 2	Band 3	Band 4	Band 5
L	2.1032	2.8544	3.4139	5.3157	0
R6	2.8063	2.5483	3.0967	5.7859	10.055
R5	3.171	2.9282	3.3487	6.6044	9.7727
R4	2.6127	3.185	2.8804	10.2528	9.5183
R3	2.4769	2.8682	2.9145	8.9754	10.018
R2	2.4474	2.7331	2.7552	4.3125	9.116
R1	2.3732	2.5306	2.3171	3.0308	9.693

Table B.2: Gene copy and transcript numbers of the biomass obtained from qPCR and their statistical comparison

	Gene copy		transcript number	
	Average per ng DNA	STDEV per ng DNA	Average per ng RNA	STDEV per ng RNA
Digester 2	15436	6796	9710	3710
Digester 3	24271	6136	20700	16400
Digester 5	14193	9689	7490	2680
	t-value	p-value	t-value	p-value
Control and Co-Digestion 1	1.6713	p= 0.170	1.1321	p=0.321
Control and Co-Digestion 2	0.1819	p=0.864	0.8402	p=0.448
Co-Digestion 1 and Co-Digester 2	-1.5220	p=0.203	-1.3769	p=0.241